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INVESTIGATION OF THE EFFECT OF LOW THRUST LEVELS ON THE BASE PRESSURE OF A CYLINDRICAL BODY AT SUPERSONIC SPEEDS

by

T. A. Martin C. E. Brazzel

May 1970

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U.S. ARMY MISSILE COMMAND

Redstone Arsenal, Alabama



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DA Project No. 1M262301A206

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Abstract

Results of supersonic wind tunnel tests are presented which show the effects of varying nozzle geometry, location, and supply pressure on the base pressure of a cylindrical body at zero angle of attack. The purpose of the tests was to investigate the parametric influences in the regions where base pressure is near a minimum, which occurs in the lower range of thrust levels. A bibliography of related experimental results is also included.

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I. Introduction

The base drag on a missile with thrust is generally greatest at low thrust levels and is significantly influenced by the various rocket nozzle geometric parameters. For clarifying the influences of the nozzle geometric parameters, a series of supersonic wind tunnel tests has been conducted with a cylindrical body by using cold, dry air to simulate the rocket exhaust. Nozzle parameters varied were diameter, expansion ratio and expansion angle, longitudinal position, and thrust level.

The basic results of the tests (base pressure variation with nozzle chamber pressure) are presented in plotted form without detailed analysis, but they are arranged to illustrate major parametric influences. These results are repeated in tabular form, and additional nozzle flow parameters and test condition information are shown in the appendix.

2. Apparatus

The model was mounted to the tunnel topwall and aligned with the tunnel flow by means of a fixed swept strut which also provided routing of the instrumentation lines and cold air supply used to simulate the exhaust flow. The external shape of the model was defined by a 4-caliber tangent-ogive nose plus a cylindrical body which wis 2 calibers long. Details of the model are shown in Figure 1.

Two types of base configurations were used during these tests. One model configuration, designated as the "open base" configuration, contained an active nozzle mounted concentrically in a larger inactive nozzle. This configuration presented considerable base area which was not adjacent to the region where the exhaust was exiting from the model. Also, this configuration was constructed so that the exit plane of the active nozzle was located at positions other than the plane of the model base. This configuration was made by combining the nozzles (Figure 1b) and the "open base" body (Figure 1a).

The model configurations designated as "closed base" were made by installing the nozzles, including sonic (Figure 1c), conical supersonic (Figure 1d), and contoured supersonic (Figure 1e) into the body identified in Figure 1a as the "closed base" body.

Tunnel No. 1 of the Ballistic Research Laboratories is a continuous flow, supersonic wind tunnel capable of operating over the Mach number range of

1.20 to 5.0. The test section dimensions are 13 by 15 inches. The minimum test Mach number for this model in this facility is 2.5. Complete details of this facility are given by Baughman.

The estimated range of inaccuracy of all data presented herein is as follows:

Mach number, ±0.008 Local model pressure, ±0.100 psi Air supply pressure,

0 to 15 psi range ± 0.030 psi 0 to 100 psi range ± 0.200 psi 0 to 300 psi range ± 0.600 psi

3. Presentation of Data

The information presented here consists of:

- a) Justification for direct comparison between results obtained with open and closed base configurations
- b) Observations on the insignificant influence of Reynolds number over the test Reynolds number range
- c) Plotted basic results arranged to illustrate major parameteric influences
- d) Tabulated results.

A detailed listing of the test condition, test configurations, base pressure, and base pressure coefficient variation with nozzle chamber pressure, thrust coefficient (CT), and momentum flux ratio (RMF) is presented in the appendix. The values of CT and RMF have been calculated by using measured values, nozzle physical dimensions, and one-dimensional flow relationships. An index to the tabulated data and symbol notation as used in this tabulation are also shown in the appendix.

Two cylindrical body configurations were tested: a closed base configuration and an open base configuration, which simulated an inactive large boost

¹ Baughman, L. E., and Kochendorfer, F. D., "Jet Effects on Base Pressures of Conical Atabodies at Mach 1.91 and 3.12," NACA RM E57E06, August 1957

nozzle surrounding an active small sustainer nozzle (Figure 1a). A comparison of results from each of the bodies with identical nozzles is shown in Figure 2. This comparison indicates that effects due to base configuration difference are very slight. On the basis of this comparison, no further reference to the base difference will be made. Excellent repeatability of data acquired in separate test entries is also shown in Figure 2.

A group of nozzles were tested at a Reynolds number lower than the nominal value to extend the range of thrust level. The results are presented in Figure 5 together with results obtained at the nominal Reynolds number. In these results there is a slight but consistent shift in the base pressure ratio at comparable chamber pressure ratios, although different chamber pressures were used to produce the comparable ones. To investigate this shift in base pressure, further testing was conducted both over a greater Reynolds number range and without the standard boundary layer transition strip on the nose. These data, presented in Figure 3, show no consistent trends with Reynolds number over the range in question ($R_N \approx 0.20$ to 0.50 million per inch). On the basis of this observation, it is felt that the shift is due to data acquisition errors and is not a Reynolds number effect.

The basic results from the test are presented in Figures 4 through 19. The nozzle configuration variable for each group of data is shown in Table I.

TABLE I. NOZZLE CONFIGURATION VARIABLES

Configuration Variable	Configuration Constants	Figure No.
Nozzle Mach	$\Gamma */DB = 0.141, \theta_{j} = 0 \text{ deg}$	4
No.	$\theta_{i} = 0 \text{ deg}, D_{i}/D_{B} = 0.20$	5
	$\theta_{j} = 20 \text{ deg}, \ D_{j}/D_{B} = 0.20$	6
Nozzle Expansion	$M_{i} = 1.78, D_{i}/D_{B} = 0.20$	7
Angle	$M_i = 2.20, D_i/D_B = 0.20$	8
	$M_i = 2.70, D_i/D_B = 0.20$	9
	$M_j = 3.20, D_j/D_B = 0.20$	10

TABLE I. NOZZLE CONFIGURATION VARIABLES (Concluded)

Configuration Variable	Configuration Constants	Figure No.
Nozzle Exit Diameter	$M_{j} = 1.0, \ \theta_{j} = 0$ $M_{j} = 1.78, \ \theta_{j} = 0$ $M_{j} = 1.78, \ \theta_{j} = 20$ $M_{j} = 2.70, \ \theta_{j} = 0$	11 12 13 14
	$M_{j} = 2.70, \ \theta_{j} = 20 \text{ deg}$ $M_{j} = 3.20, \ \theta_{j} = 0 \text{ deg}$	15 16
Nozzle Exit Position	Nozzle, $D_j/D_B = 0.1$ Nozzle, $D_j/D_B = 0.2$ Nozzle, $D_j/D_B = 0.3$	17 18 19

The symbols used in these figures are identified in the following list, while those used with the tabulated data are given in the preface of that section.

$D_{\overline{B}}$	Reference diameter of model
D _i	Diameter of nozzle at exit plane
M_{i}	Mozzle design Mach number
M_{∞}	Free stream Mach nun ber
р _е	Jet stagnation pressure
р _В	Mean base pressure
p _∞	Free stream static pressure
R_{N}	Reynolds number per inch
X _n	Location of nozzle exit plane relative to model base, negative rearward
θ .	Half-angle divergence of nozzles

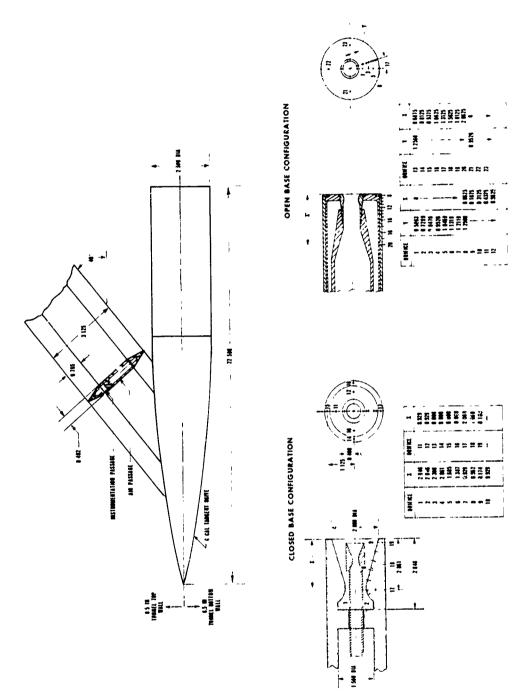


FIGURE 1. MODEL DETAIL

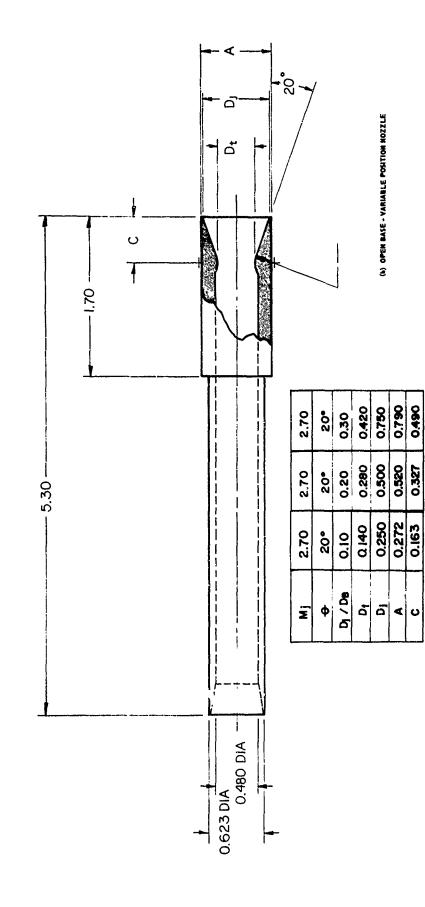
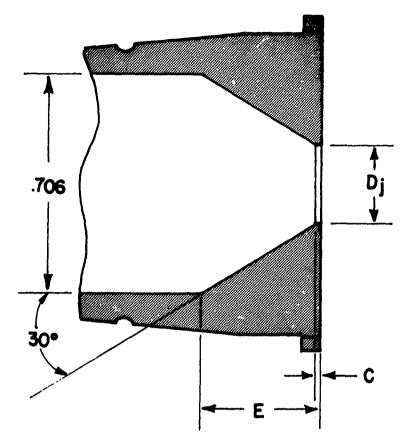


FIGURE 1. MODEL DETAIL (Continued)

CLOSED BASE SONIC NOZZLE



Mj	1.0	1.0	1.0
0		-	*******
Dj/DB	0.100	0.140	0.200
Dj	0.250	0.352	0.500
С	0.010	0.010	0.010
E	0.404	0.302	0.191

(c) SONIC NOZZLES

FIGURE 1. MODEL DETAIL (Continued)

CLOSED BASE COMICAL MOZZLE

←å →

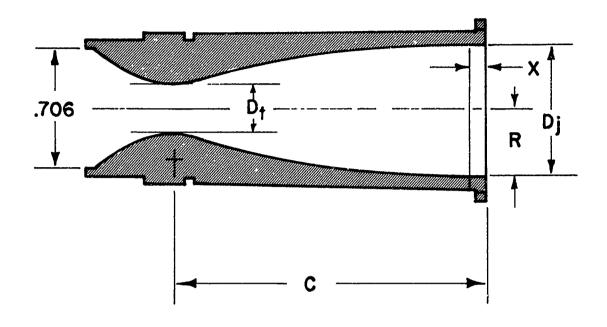
902

45

1.78	8	1.78	1.78	1.78	2.20	2.70	2.70	2.70	2.70	3.20	3.80
3	53	20•	200	20•	200	• 01	15•	20•	20	20•	20•
ķ	8	<u>8</u>	200	300	200	.200	.200	.200	300	.200	200
4.	420	209	.420	630	.353		80.	280	.420	.221	.167
ιÿ	8	.250	500	750	500	Ľ	.500	.500	.750	.500	.500
4.	464	.075	. 143	.221	.233	929	.429	.327	.491	.403	472

(d) CONICAL NOZZLES

FIGURE 1. MODEL DETAIL (Continued)



CLOSED BASE
CONTOURED NOZZLES

Mj	1.78	1.78	2.20	2.70	2.70	3.20	3.20
ф	0	0	0	0	0	0	0
Dj/D _B	.168	.200	.200	.200	.252	.200	.320
Dt	.352	.420	.352	.280	.352	.220	.362
Dj	.420	.500	.500	.500	.629	.500	.800
С	.591	.703	.909	1.096	1.382	1.249	1.996

(e) CONTOURED NOZZLES

FIGURE 1. MODEL DETAIL (Concluded)

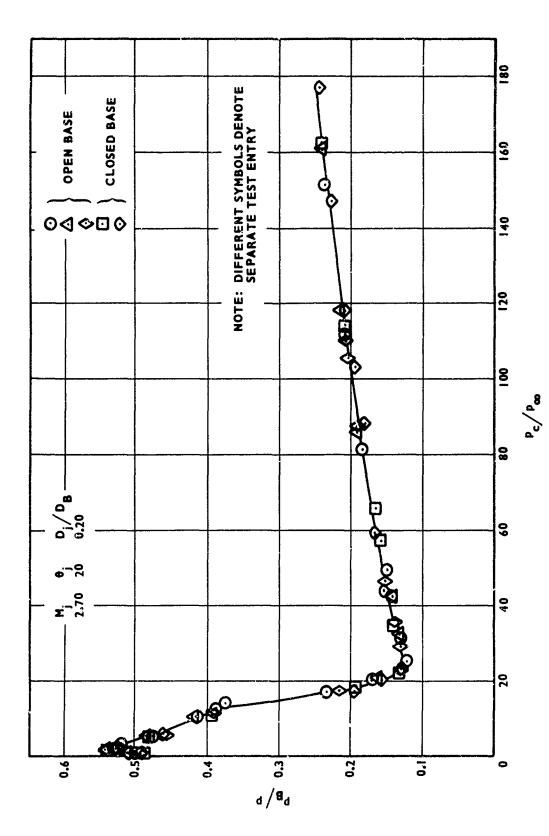
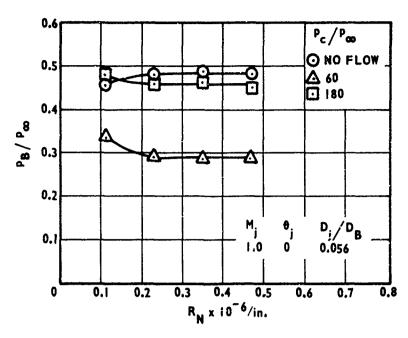
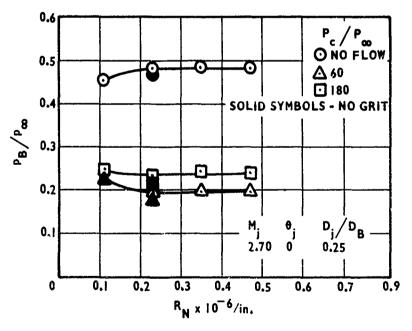


FIGURE 2. BASE PRESSURE FOR OPEN VERSUS CLOSED BASE CONFIGURATIONS



a. SONIC NOZZLE



b. SUPERSONIC NOZZLE

FIGURE 3. REYNOLDS NUMBER EFFECT ON BASE PRESSURE

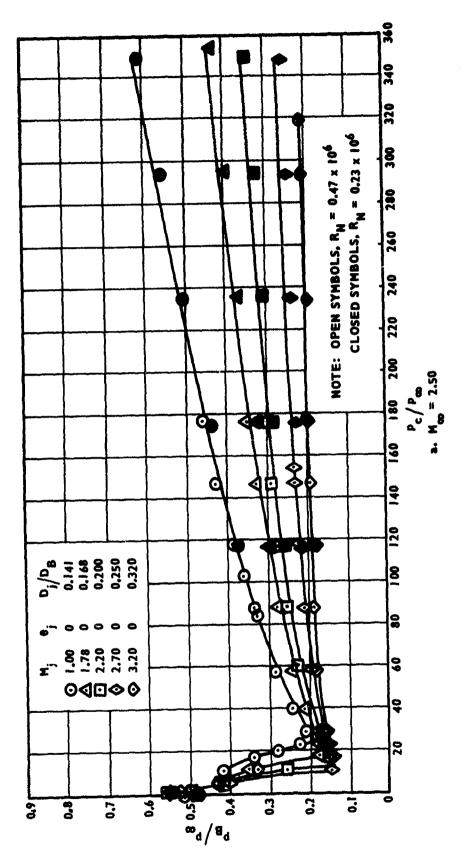


FIGURE 4. EFFECT OF JET MACH NUMBER ON BASE PRESSTRE, CONSTANT THROAT DIAMETER

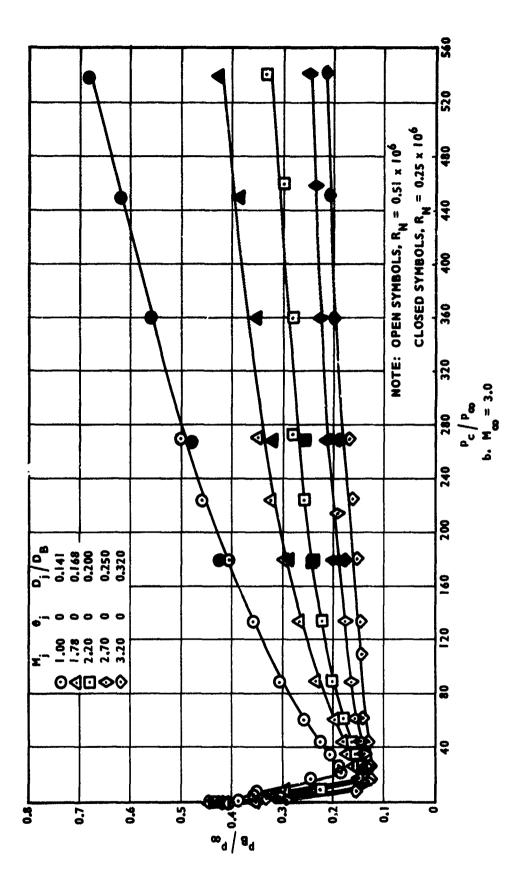


FIGURE 4. EFFECT OF JET MACH NUMBER ON BASE PRESSURE, CONSTANT THROAT DIAMETER (Concluded)

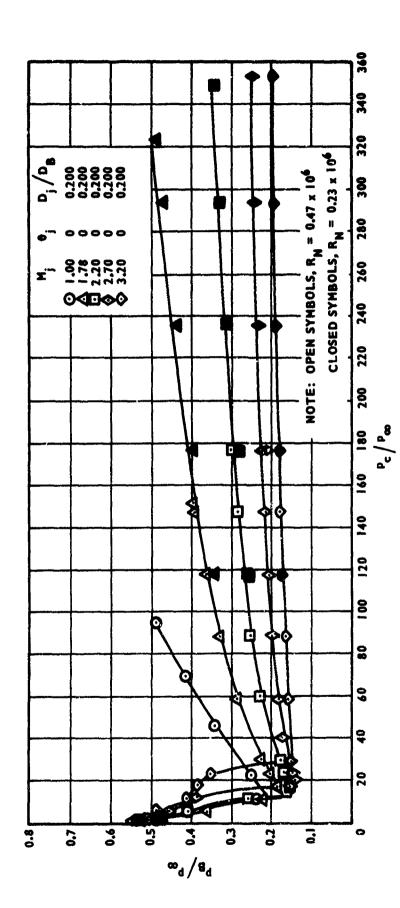


FIGURE 5. EFFECT OF JET MACH NUMBER ON BASE PRESSURE, CONTOURED NOZZLES, CONSTANT EXIT DIAMETER

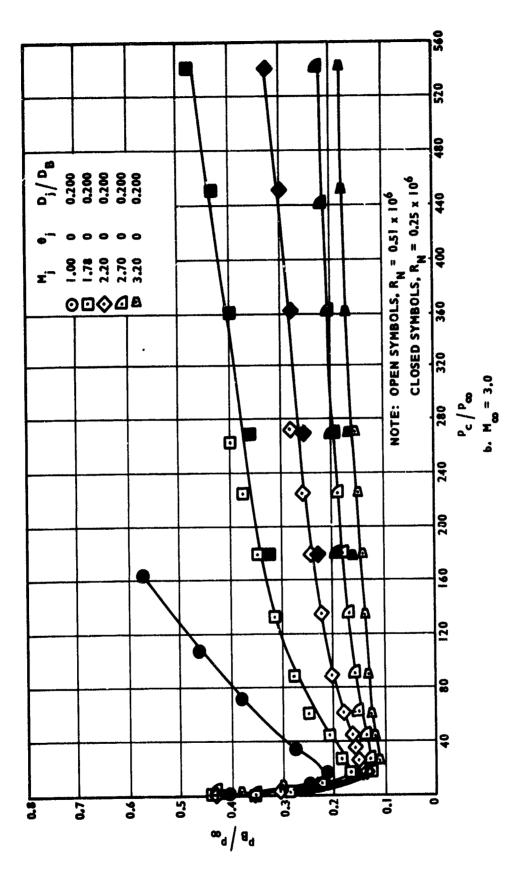
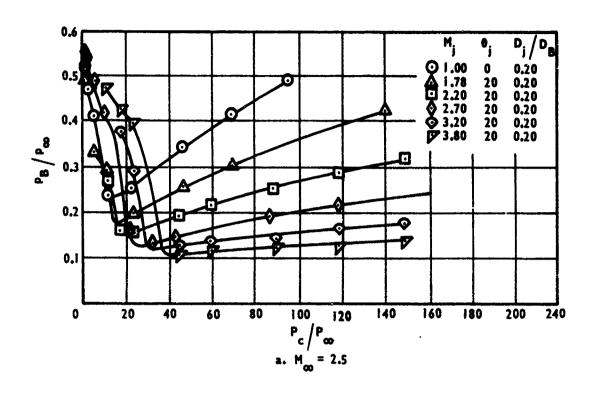


FIGURE 5. EFFECT OF JET MACH NUMBER ON BASE PRESSURE, CONTOURED NOZZLES, CONSTANT EXIT DIAMETER (Concluded)



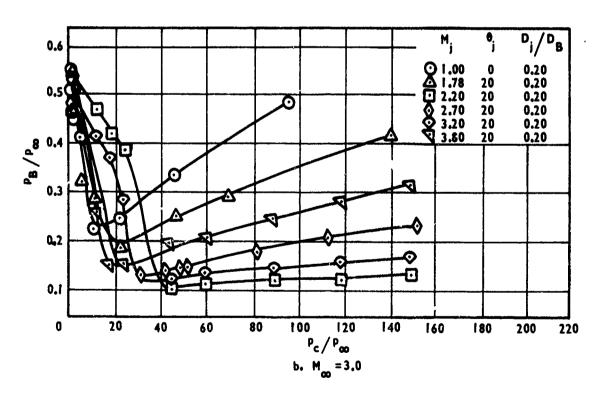
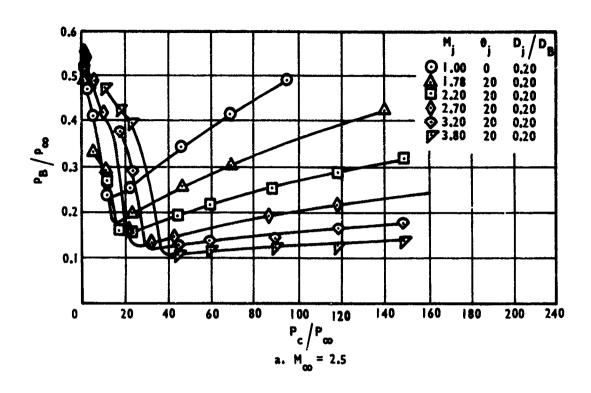


FIGURE 6. EFFECT OF JET MACH NUMBER ON BASE PRESSURE, CONICAL NOZZLES, CONSTANT EXIT DIAMETER



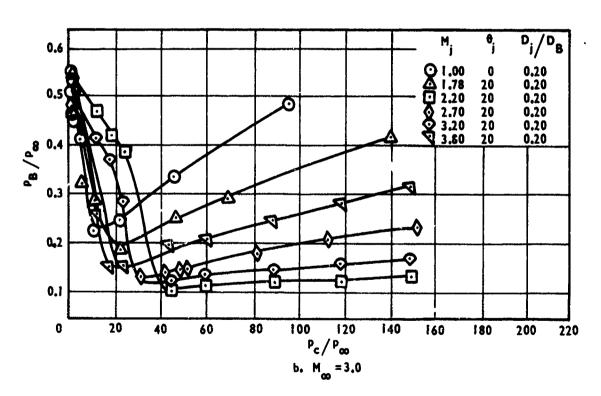
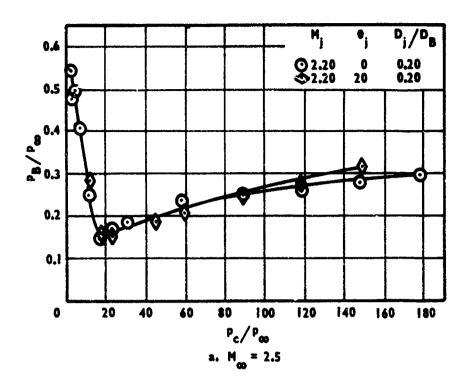


FIGURE 6. EFFECT OF JET MACH NUMBER ON BASE PRESSURE, CONICAL NOZZLES, CONSTANT EXIT DIAMETER



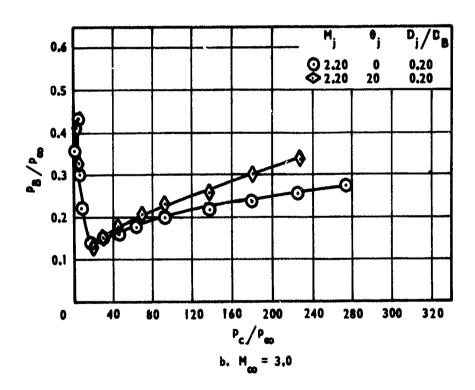
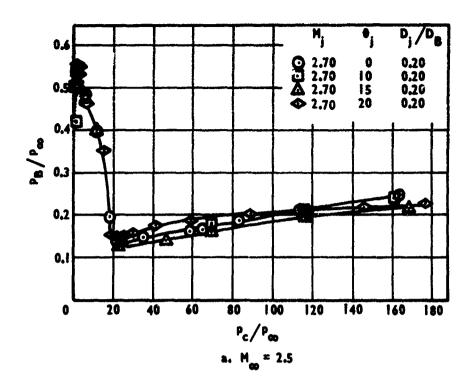


FIGURE 8. EFFECT OF NOZZLE ANGLE ON BASE PRESSURE, EXIT MACH NUMBER = 2.20



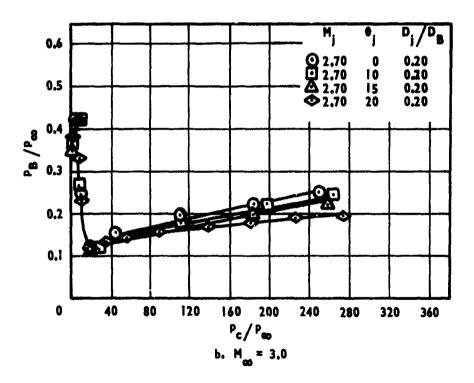
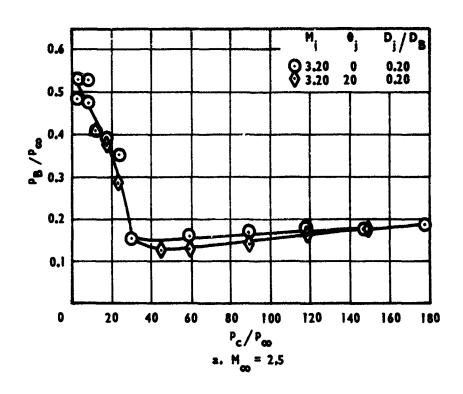


FIGURE 9. EFFECT OF NOZZLE ANGLE ON BASE PRESSURE, EXIT MACH NUMBER = 2.70



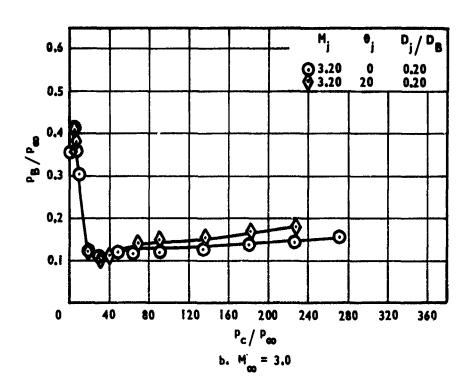
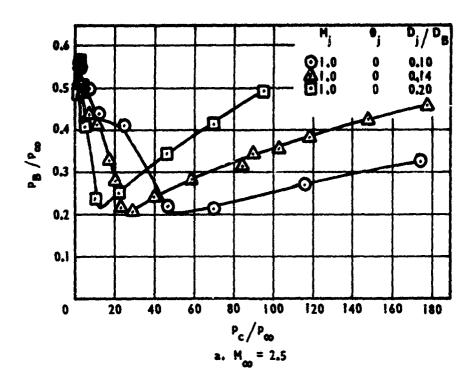


FIGURE 10. EFFECT OF NOZZLE ANGLE ON BASE PRESSURE, EXIT MACH NUMBER = 3.20



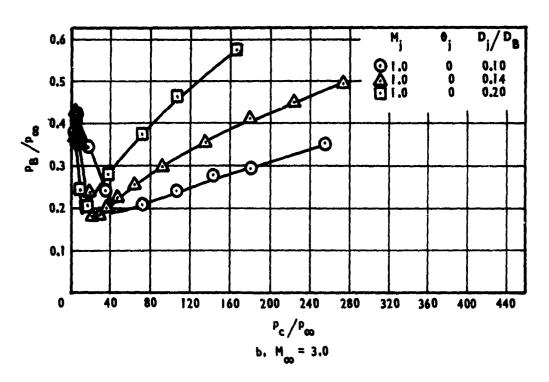
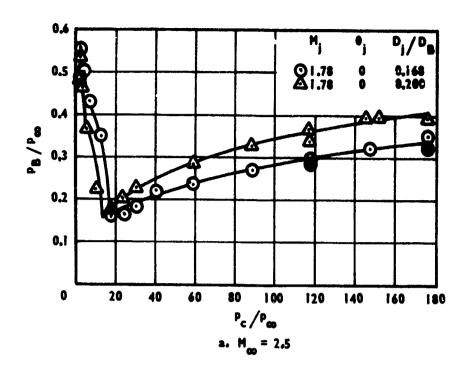


FIGURE 11. EFFECT OF NOZZLE DIAMETER ON BASE PRESSURE, EXIT MACH NUMBER = 1.00



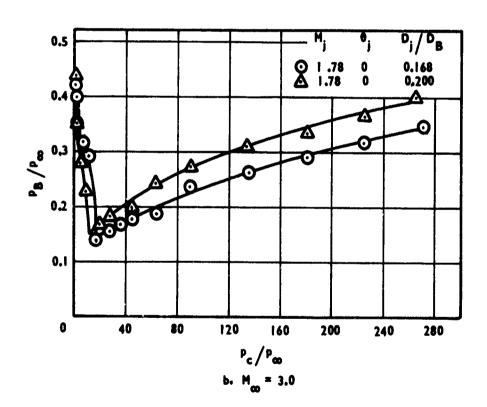


FIGURE 12. EFFECT OF NOZZLE DIAMETER ON BASE PRESSURE, EXIT MACH NUMBER = 1.78, CONTOURED NOZZLES

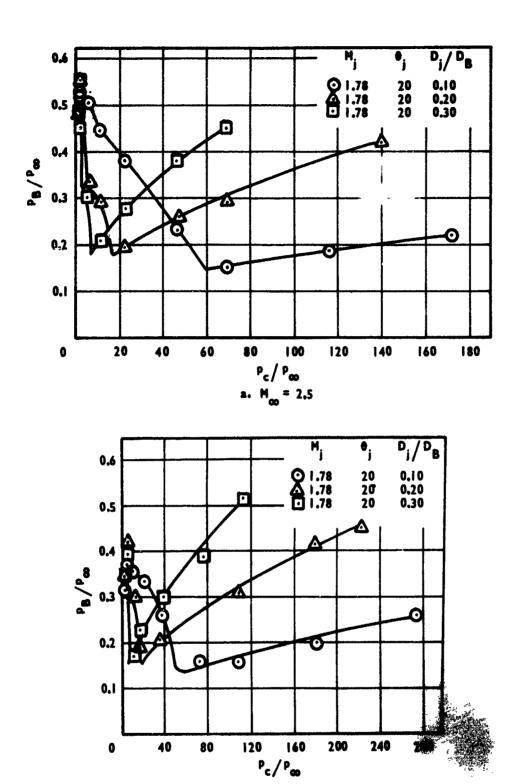


FIGURE 13. EFFECT OF NOZZLE DIAMETER ON BASE PRESSURE, EXIT MACH NUMBER = 1.78, CONICAL NOZZLES

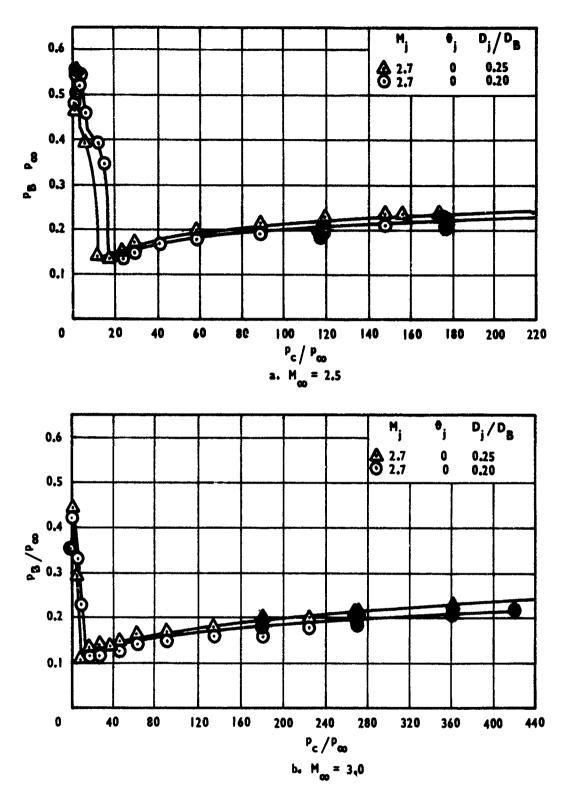
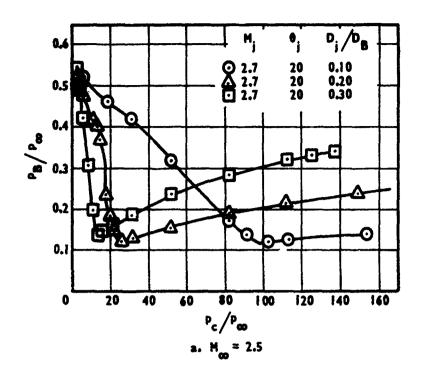


FIGURE 14. EFFECT OF NOZZLE DIAMETER ON BASE PRESSURE, EXIT MACH NUMBER = 2.70, CONTOURED NOZZLES



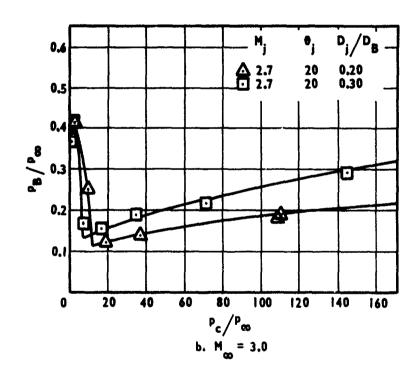
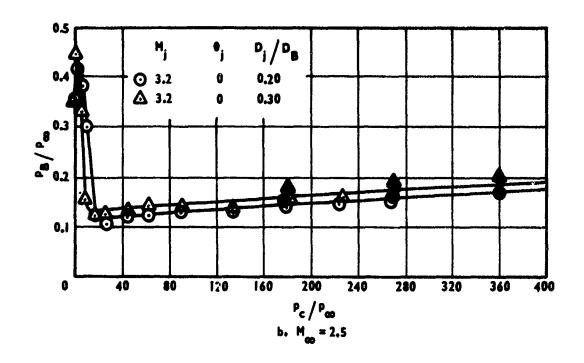


FIGURE 15. EFFECT OF NOZZLE DIAMETER ON BASE PRESSURE, EXIT MACH NUMBER = 2.70, CONICAL NOZZLES



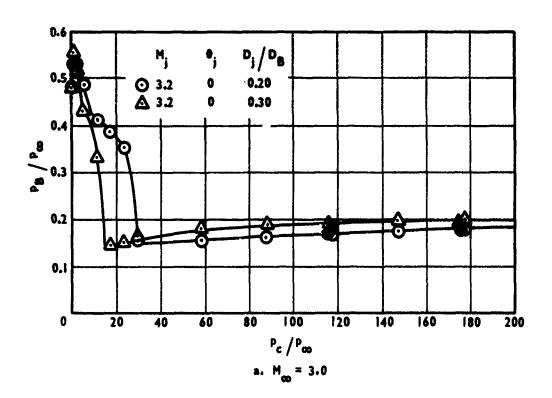


FIGURE 16. EFFECT OF NOZZLE DIAMETER ON BASE PRESSURE, EXIT MACH NUMBER = 3.20

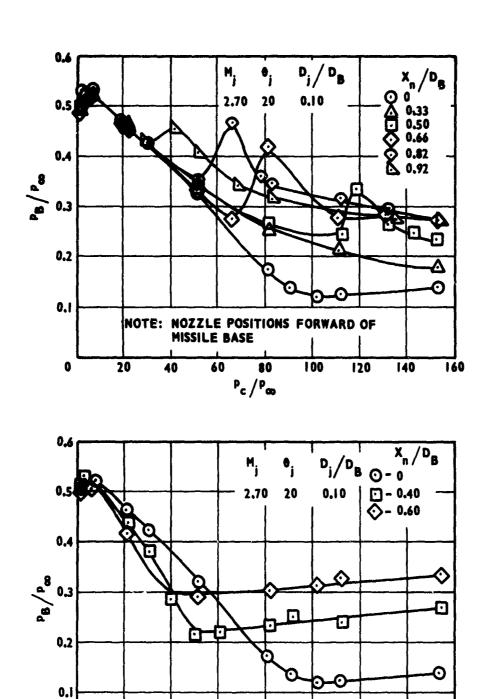


FIGURE 17. EFFECT OF NOZZLE POSITION ON BASE PRESSURE, NOZZLE-BASE RATIO = 0.10, MACH NUMBER = 2.50

NOTE: NOZZLE POSITIONS REAR OF MISSILE BASE

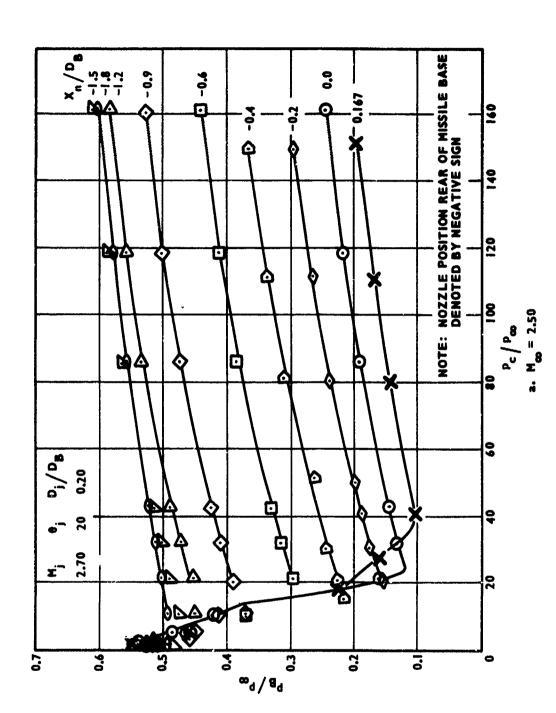
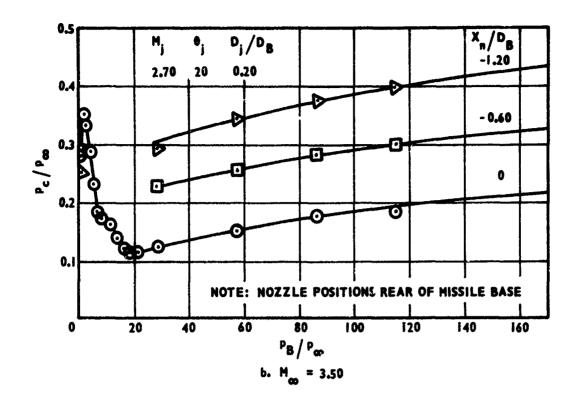


FIGURE 18. EFFECT OF NOZZLE POSITION ON BASE PRESSURE, NOZZLE-BASE RATIO = 0.20



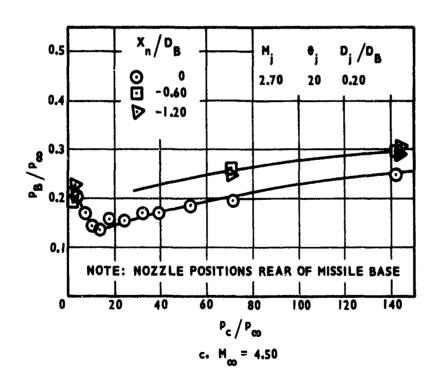


FIGURE 18. EFFECT OF NOZZLE POSITION ON BASE PRESSURE, NOZZLE-BASE RATIO = 0.20 (Concluded)

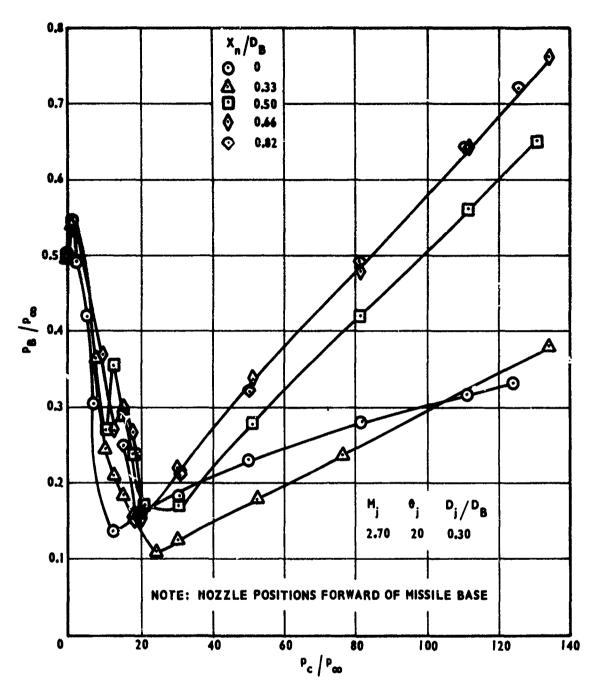


FIGURE 19. EFFECT OF NOZZLE POSITION ON BASE PRESSURE, NOZZLE-BASE RATIO = 0.30, MACH NUMBER = 2.50

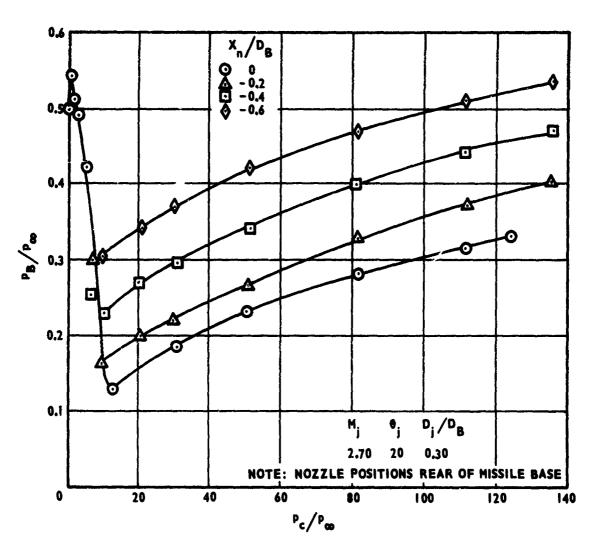


FIGURE 19. EFFECT OF NOZZLE POSITION ON BASE PRESSURE, NOZZLE-BASE RA TIO = 0.30, MACH NUMBER = 2.50

Bibliography

- Cortright, E. M., Jr., and Schroeder, A. H., "Investigation at Mach Number 1.91 of Side and Base Pressure Distributions over Conical Boattails without and with Jet Flow Issuing from Base," NACA RM E51F26, September 1951.
- Bromm, A. F., Jr., and O'Donnell, R. M., "Investigation at Supersonic Speeds of the Effect of Jet Mach Number and Divergence Angle of the Nozzle Upon the Pressure of the Base Annulus of a Body of Revolution," NACA RM L54I16, December 1954.
- Reid, J., and Hastings, R. C., "The Effect of a Control Jet on Base Pressure of a Cylindrical Afterbody in a Supersonic Stream," Report No. Aero 2621, December 1959, Royal Aircraft Establishment, Farnborough, England.
- Hendersen, J. H., "Jet Effects on Base Pressures of Cylindrical and Flared Afterbodies at Free-Stream Mach Numbers of 1.65, 1.82, and 2.21," ARGMA TR 1G3R, June 1960, Army Rocket and Guided Missile Agency, Ordnance Missile Laboratories, Division, Systems Analysis Laboratory, Redstone Arsenal, Alabama.
- Craven, A. H., Chester, D. H., and Graham, B. H., "Base Pressure at Supersonic Speeds in the Presence of a Supersonic Jet," CoA Report No. 144, AD No. 260621, December 1960, The College of Aeronautics, Cranfield.
- Charczenko, N., and Hayes, C., "Jet Effects at Supersonic Speeds on Base and Afterbody Pressures of a Missile Model Having Single and Multiple Jets," NASA TN D-2046, November 1963, Langley Research Center, Hampton, Virginia.
- Harries, M. H., "P. ssure on Axisymmetric Base in a Transonic or Supersonic Free Stream in the Presence of a Jet," Report AE-584:1, March 1967, FFA The Aeronautical Research Institute of Sweden, Stockholm, Sweden.
- Reid, J., "The Effect of Jet Temperature on Base Pressure," Royal Aircraft Establishment Technical Report 68176, July 1968.

Appendix Tabulated Test Results

The following data were listed from computer equipment and the symbols used to designate various parameters were selected to facilitate the use of this equipment. The following list identifies the symbols used in this portion of the report:

CPB CT	Base pressure coefficient, $\left[\frac{PB}{PF} - 1.0\right] \frac{1.0}{0.7 \text{ (MF)}^2}$ Thrust coefficient, thrust/[dynamic pressure × reference area]
D*	Diameter of nozzle at the throat (in.)
DJ	Diameter of nozzle at the exit plane (in.)
DB	Reference diameter of body, 2.50 in.
GJ	Jet specific heat ratio
L	Model length (in.)
MF	Free stream Mach number
MJ	Jet exit Mach number
PB	Mean base pressure (psia)
PC	Jet stagnation pressure (psia)
\mathbf{PF}	Free stream static pressure (psia)
RMF	Jet momentum flux ratio, $\frac{(PJ) (AJ) (MJ)^2}{(PF) (AB) (MF)^2}$, where $AJ = \pi \overline{DJ}^2$, $AB = \pi \overline{DB}^2$, and $PJ = \text{jet}$ static pressure
THEJ	Divergence half-angle of nozzles (deg)
TOF	Free stream static temperature (°F)
RN	Reynolds number per inch

(negative positions rear of model base)

Location of nozzle exit plane relative to model base (in.)

ХJ

The data are arranged according to the index given in Tables A-I through A-III.

TABLE A-I. INDEX TO TABULATED DATA

Group	M _j	$\theta_{f j}$	D _j /D _B	M _∞	R _N × 10 ⁻⁶
1A	1.0	0	0.10	2.50	0.47
1 1	1.0	0	0.10	3.00	0.51
1B	1.0	0	0.14	2.50	0.23
	1.0	0	0.14	2.50	0.47
	1.0	0	0.14	3.00	0.25
	1.0	0	0.14	3.00	0.51
1C	1.0	0	0.20	2.50	0.47
1 1	1.0	0	0.20	3.00	0.51
2A	1.78	0	0.16	2.50	0.23
]	1.78	0	0.16	2.50	0.47
1 1	1.78	0	0.16	3.00	0.25
	1.78	0	0.16	3.00	0.51
2B	1.78	0	0.20	2.50	0.23
	1.78	0	0.20	2.50	0.47
1 1	1.78	0	0.20	3.00	0.25
	1.78	0	0.20	3.00	0.51
2C	1.78	5	0.20	2.50	0.47
	1.78	5	0.20	3.00	0.51
2D	1.78	20	0.10	2.50	0.47
	1.78	20	0.10	3.00	0.51
2E	1.78	20	0.20	2.50	0.47
	1.78	20	0.20	3,00	0.51
2F	1.78	20	0.30	2.50	0.47
	1.78	20	0.30	3.00	0.51
3A	2.20	0	0.20	2.50	0.23
	2.20	0	0.20	2.50	0.47
	2.20	0	0.20	3.00	0.25
	2.20	0	0.20	3.00	0.51
3B	2.20	20	0.20	2.50	0.47
	2.20	20	0.20	3.00	0.51
4A	2.70	0	0.20	2.50	0.23
	2.70	0	0.20	2.50	0.51
	2.70	0	0.20	3.00	0.25
i	2.70	0	0.20	3.00	0.51

TABLE A-I. INDEX TO TABULATED DATA (Concluded)

Group	M	$\theta_{\mathbf{j}}$	D _j /D _B	M _∞	R _N × 10 ⁻⁶
4B	2.70	0	0.25	2.50	0,23
	2.70	0	0.25	2.50	0,47
	2.70	0	0.25	3.00	0.25
	2.70	0	0.25	3.00	0.51
4C	2.70	10	0.20	2.50	0.47
	2.70	10	0.20	3.00	0.51
4D	2.70	15	0.20	2.50	0.47
	2.70	15	0.20	3.00	0.51
4E	2.70	20	0.20	2,50	0.47
	2.70	20	0.20	3.00	0.54
	2.70	20	0.20	3.50	0.50
	2.70	20	0.20	4.00	0.50
	2.70	20	0.20	4.50	0.49
4F	2.70	20	0.30	2.50	0.54
	2.70	20	0.30	3.00	0.54
5A	3.20	0	0.20	2.50	0.23
	3.20	0	0.20	2.50	0.47
	3.20	0	0.20	3.00	0.25
	3.20	0	0.20	3.00	0.51
5 <u>'</u> B	3.20	0	0.31	2.50	0.23
	3.20	0	0.31	2.50	0.47
i)	3.20	0	0.31	3.00	0.25
	3.20	0	0.31	3.00	0.51
5 C	3.20	20	0.20	2.50	0.47
	3.20	20	0.20	3.00	0.51
6 <u>'</u> A	3.80	20	0.20	3.00	0.50
	3.80	20	0.20	2.50	0.47

TABLE A-II. NOZZLE POSITION DATA

Group	M _j	$\theta_{\mathbf{j}}$	D_{j}/D_{B}	M _∞	R _N (in.)	x ^N p ^B
7A	2.70	20	0.10	2.50	0.55 × 10 ⁺⁶	-0.60 -0.40 0 0.33 0.50 0.67
7B	2.70	20	0.20	2.50	0.55 × 10 ⁺⁶	0.82 0.98 -0.60 -0.40 -0.20 0 0.33 0.50
7C	2.70	20	0.30	3.50 4.50 2.50	$0.50 \times 10^{+6}$ $0.49 \times 10^{+6}$ $0.55 \times 10^{+6}$	0.67 0.82 0.98 -0.60 -1.20 -0.60 -1.20 -0.60 -0.40 -0.20 0 0.33 0.50
						0. 50 0. 67 0. 82

TABLE A-III. REYNOLDS NUMBER DATA

Group	М _ј	$\theta_{ m j}$	D _j /D _B	$ m M_{\infty}$	R _N (in.)
8B	1.00	0	0. 25	2.50	$\begin{array}{c} 0.12 \times 10^{+6} \\ 0.23 \times 10^{+6} \\ 0.35 \times 10^{+6} \\ 0.47 \times 10^{+6} \\ 0.12 \times 10^{+6} \\ 0.23 \times 10^{+6} \\ 0.35 \times 10^{+6} \\ 0.47 \times 10^{+6} \end{array}$

	00.0 0.00	RN/1N	40.00 60.00 60.00	000000000000000000000000000000000000000		00*0 90/fx	RN/1N	1C 60.00 60.00	0000	00.09		
	80/50	LFN6TH 15.0	-001 -002 -016			03/08	LENGTH 15.0	003*	1.005 1.343 1.679	1.992		
	69.	63	.0001. .0010 .0050	.0210 .0420 .0630 .1050 .1500		0J •35	1.40	.0004*	.2940 .3930	.5820		
	0* •25	PF 1.11	CPB 1011 0931 1028	1267 1257 1216 1127 1163		•35	PF .85	CP8 -,1195	1272 1125 1003	0882		
	1HEJ 0.00	100 100.00	P8/PF •3682 •4178 •3571	.2450 .2141 .2403 .2955 .3503		THE.J 0.00	T0F 93.00	P8/PF .4767	.5075 .5075	.6140		
<	1.00	3.00	PC/PF .38 1.81 9.14 18.05	35.94 107.53 107.43 180.33 255.85 144.55		H.1	NF 2.50	PC/0F .49 117.29	234.58 293.05	347.57		
GROUP					GROUP 18							
	00°0	RN/18	63.00 63.00 63.00	63.00 63.00 63.00 63.00		xJ/D8 0.00	RN/1N .47	10 60.00 60.00	0000	00.09	000000000000000000000000000000000000000	60.00 60.00 60.00 60.00
	80/FU	LENGTH 15.0	.001 .002 .013	. 131 . 139 . 333 . 500		03/08	LENGTH 15.0	CT 003* 003*	.005	.029 .062 .096	.130 .229 .330	.503 .587 .673 .841
	03 •25	1.40	. 0005*	. 0190 . 0380 . 0580 . 1460		6J •35	6.1 1.40	.0004*	0050	.0190 .0290	.0390 .0490 .0680 .0970	.1480 .1720 .1970 .2460
	0*	PF 1•73	CPB 1071 1080 1176	-1387 -1831 -1828 -1702 -1587		9* •35	PF 1.69	CPB1175	-1053 -1134	1307 1334 1510	-1169 -11608 -11640 -11533	1517 1466 1416 1319 1244
	THE J 0.00	107.10F	98/9F .5416 .5378 .4966	2168 2168 2169 2694 3238		THE, 0.30	10F 93.70				.2257 .2089 .2399 .2822	
	M 1	2.50	PC/PF 1-15 1-73 5-50	23.03 46.08 69.71 115.88 173.62			2.50	PC/PF •49 •58	1.76	5.86 11.74 17.60 20.65	23.54 29.39 40.68 58.31	88.39 103.10 117.99 147.32 176.80

HJ HF HF 3.00 PC/PF 9.00 1.81

725 7.00 8N/IN .25 .25 .25 60.00 60.00 60.00 XJ/DB 0.00 0.00 RN/IN .53 TC 68.00 68.00 68.00 68.00 68.00

MJ 1.00 MF 2.50 .49 .11 1.14 1.15 2.59 5.47 11.22 5.47 11.22 5.47 6.06 6.06 6.06 6.06

00°0	RN/IN	10	00.09	60.00	00.09	90.00	•								80/Cx	8	RN/18	,	, č	00.04	00.09	00.09										
03/08	LENGTH 15.0	C.1	. 733	1.104	1.475	7.213									80/50	•	LF>H 15.0	ţ	787	12.174	1.570	1.966	2.350									
54.	63	RMF 0000**	.3020	06570	.6040	0400	•								0.0		1.40	u 3	0128	4800	.6420	.8030	.9640									
0* •35	85	CPR	1614	1524	1440	1300	•								0.4		PF • 55	893	-,1131	-1080	1027	0973	0912									
1HFJ 0.00	10F 93,30	P8/PF	.2936	.3332	.3696	, 104.	•								1 HE 3		10F 93.10	PRIPE	-2869	.3193	.3525	.3869	.4250									
M.J. 8.78	MF 2.50	PC/PF	117.64	176.48	235.54	352.83									MJ 1.78	;	3.00	PC/PF	180.52	269.74	360.39	450.68	540.92									
00.00 0.00	417 . 47	1C 60.00	00.09	40°00	60.00	60.00	60.00	60.00	60.00	60.00	90.00	00.00	00.00	00.00	90/fx		88/1N .51	2	90.00	00.09	40.00	00.09	60.00	00*09	00*09	00.09	60.00	60.00	00.00	00-09	00.00	00.00
03/08 • 16	LFN6TH 15.0	CT 004*	-*005¢	-012	790.	.104	.142	.179	642.	.364	****	950	1.106	¢	03/DB		LFN6TH 15.0	13	003*	-*005*	00000	•015	•034	.073	.113	-152	192	.268	. 390	.586		1.180
67 • • • •	6.1 1.40	RMF.	.0016€	0000	0300	.0450	0090*	.0750	.1040	01410	0677.	3780	09.54		DJ •42	. (1.40	RMF	*6000	*8000*	.0017*	.0080	.0150	.0320	• 0480	.0640	0800	.1110	.1610	2210	0176	.4830
0* •35	PF 1.69	CPB 1159	1020	1134	1481	1888	1891	1862	1798	1131	7001-	1546	- 1493		0* •35		1.10	843	1024	0911	0934	1080	1112	-,1356	1334	1316	1302	1211	-121.	1166	1031	1033
THEJ 0.00	10F 93.10	PB/PF	.5537	.5034	.3518	.1736	.1724	. 1853	.2132	27391	2007	3234	3464		THF.J	Č	93.00															.3489
1.78	7.50 5.50	PC/PF .49	1.18	2.94	11.81	17.69	23.59	26.62	80.03	90.90	117.67	147.32	176.83		M.)	1	3.00	PC/PF	.38	8.	1.81	4.52	8.93	17.95	26.99	36.03	45.10	95.39	8.5	180.34	226.60	271.23

00.00 00.00	RN/18	70 60.00 60.00 60.00 60.00 60.00 60.00	xJ/08 0.00 255 75 60.00 60.00 60.00	
13/08	LFNGTH 15.0	CT 	DJ/08 -20 LENGTH 15-0 1-662 2-784 2-784 3-343	
09 • 50	63	RMF .0010° .6420 .8570 1.0670	6.5 6.7 1.40 8.45 6.455 6.455 6.455 1.1380 1.1380	
0" •42	94 8.	CP8 1194 13487 1782 1782 1783	0.47 0.47 0.47 0.1011 0.1013 0.0193 0.01934	
THFJ 3.30	10F 93.30	PB/PF • 4173 • 3483 • 433 • 4935	THE J 1.00 TOF 93.00 PR/PE .3551 .3673 .3674	
мј 1.78	MF 2.50	PC/PF 117-66 117-66 117-66 135-46 235-72 293-34 372-80	HJ 1.78 3.00 PC/PF 187.18 765.52 365.52 365.52 365.63 547.97	
xJ/DA 0.30	47	60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00	16.12x 16.04	
03/08	LENGTH 15.0		15.0 15.0 15.0 15.0 15.0 10.03	
09°	6.1 1.40		0.50 1.40 RMF 0.0015 0.0010 0.027 0.02	
0* •42	9F 1.69	CPB 1191 1056 1220 1773 1773 1770 1530 1531	0.47 PF 1.10 C.D.A 1022 1024 1124 1126 1126 1126 1126 1126 1126	:
THEJ 0.00	TOF 93.10		THE) 0.10 10.30 110.93.30 2484 2784 2784 2784 2784 3126 3126 3433	•
1.78	2.50	PC/PF - 49 1.17 1.17 5.68 11.64 11.64 11.64 11.33 58.75 58.75 58.75 46.92	HJ 10-78 HF 30-70 C/PF 0-38 0-71 18-73 45-25 65-45 65-45 180-85 180-85 180-85	. 1 • ()

83/08 0.00 84/18	65.00 65.00 65.00 65.00 65.00 65.00	60.0 50.0	8N/IN .51	1C 665.00 665.00 665.00 665.00 665.00
03/08 • 20 LENGTH		80/c0 10	LENGTH 15.0	CT001* 000* 012 026 054 169 165 177 177
20 04.	.0005* .0005* .00210 .0840 .1820 .3640	25.	1.40	RMF • 00004 • 00006 • 0050 • 0020 • 0080 • 1130 • 1710
0. 4. 4		D*	1:11	CPB 1008 1008 1061 1133 1337 1272
147,1 5.00 10F	PB/PF .3689 .4172 .2614 .1600 .1948 .2430 .3364	THEJ 20.00	10F 133.30	PB/PF • 3299 • 3827 • 3827 • 2837 • 1627 • 1658 • 2550
1.78 1.78	PC/PF 0.39 1.79 17.45 17.45 144.38 144.38	UP 2D	MF 3.00	PC/PF • 41 1 9 91 9 815 36 10 72 04 180 811 180 811 180 891
		GROUP		
x3/D8 0.00 RN/IN	TC 73.00 73.00 73.00 73.00 73.00 73.00	00°0 90/fx	RN/1N	70.00 70.00 70.00 70.00 70.00 70.00 70.00 70.00
0J/DB .20 LENGTH 15.0		63/C0 01.08	LENGTH 15.0	CT 001* 001* 0-0000* 0-0000* 0-0000* 0000 0000 151
05. 05.	RMF .00094 .00204 .0200 .0410 .0410 .0400 .3380	63 525	6.1	RMF .0002* .0005* .0012* .012* .0100 .0200 .0420 .1050
0. 6. 79. 19.		D*	PF 1.73	CPB 1205 1077 1092 1148 1705 1705 1705 1902
1265 5.00 106	84/87 6447 6347 6347 61434	тнғ. 27.0		PB/PF • 4843 • 5395 • 5334 • 5474 • 2355 • 1875 • 1875
1. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7.	PC/PF 10.57 110.40 23.17 456.58 119.02	1 °	4F 2.50	PC/PF 1014 1014 1014 1016 1016 1016 1016 1016

GROUP 2C

00°0	RN/1N	65.00 65.00 65.00	65.00	65.00 65.00		90/fx	RN/IN	16.	67. 50.	67.00	67.00	67.00	67.00	00.10	
02.	LENGTH 15.0	0.005# 0.000*	.215 .666	1.113		03/08	LENGTH	15.0	011*	002*	.232	-485	999	167-1	
.50	1.40	.0005*	0450	.5350		L0 .75	ટ	1.40	.0012*	.0055	1000	.2030	.4130		
0*	PF 1-11	CPB 1072 0934	-1288	0938		D*	4	= {	1013	0964	1246	1133	9960-	-0143	
THEJ 20~30	107 100.001	PB/PF •3679 •4165	2766	.4132 .4528		THF.3	TOF	100.00	98/PF •3689	.3992	.2239	.2941	.3971	•5135	
м. 1.78	MF 3.00	PC/PF -38 1-79	35.87 10.8.4 10.8.57	180.75	GROUP 2F	L#	H.	3.00	96/2d 939	1.78	17.71	35.87	72-79	111.40	
90/fx	RN/1N	1C 63.00 63.00	63.00 63.00 63.00	63.00 63.00 63.00		×3/08	00.00	N1/N2 - 47	70	70.00	70.00	70.00	00.00	20.00	70.00
03/08	LENGTH 15.0	CT 006*	.038	.404 .610 1.239		80/F0	• 30	LENGTH 15.0	5	015*	*00*	680	207	910	1.367
03 .50	6.1 1.40	PMF .0009*	.0190 .0410	.1680 .2520 .5090		3	.75	1.40	RMF	.0022*	.0110*	.0450	0260.	3790	.5660
*4	PF 1.73	CPB 1195 1044	1556 1653 1894	1740 1630 1350		# G	• 63	PF 1.73	863	1192	1281	1626	1853	-1458	1282
THES	TOF 130 • 30	98/PF -4875	.3333 .2919 .1947	.2548 .3719 .420?		H	00°02	107 • 90	P8/PF	4888	.4513	.3038	.2364	1975	4507
H .	* 5	PC/PF	5.35	46.34 69.44 139.99		ā	1.78	2.50	PC/PF	8.	2.44	5.50	11.35	23.26	200

x3/08 0.00	4N/1N	2	40.00	00.09	00.09	60.00	00.09	60.09										2	8	KN/1N	.25	:	کو و	00.09	00.04	90.09	90.09										
02. .20	LENGTH 15.0	ij	-,000	.774	1.164	1.560	1.945	2.305											.20	LENGTH	15.0	;	40	1.263	1.661	2.077	2.495										
09• •	1.40	1	•6000•	.3419	.5110	.6830	.8510	1.0080										ä	. 50	3	1.40	1	M .	0296	0746	0806	1.0900										
0* •35	g . ñ ec		-1196	1692	1629	1575	-1536	1496										å	•35	n d	.55		84. 86.			01110	1070	: :									
THFJ 3.30	T0F		4766															1	0.00	107	93.00		PB/PF	.2311	1867.	20.3	2262										
M.5	Ξ,	2 :	PC/PF	117.80	176.44	226.08	40 500	04.642	C1.01C									:	2 × 30	1	3.00		PC/PF	180.43	2.01.28	10101	76 179										
x3/D8	RN/1N	.47	10	00.09	00-09	60.09	60.00	90.09	50.00	00.09	00.09	90.09	60.09	60.00	00.09	60.00			xJ/08 0.00		RN/IN	.51	70	60.00	60.00	60.00	90.09	00.09	00.09	00.00	00.00	00.00	00.00	00.04	00.09	60.00	00.09
90/00	. 20 LFN6TH	15.0	5	+900	-*003*	•003	• 030	690*	.108	.147	.187	• 383	.579	.776	696*	1.167			03/08	1	LFNGTH	15.0	Ę	005#	003	*00U*U	•014	•034	•076	• 110	. 160	102	187	114.	1100	1.034	1.257
2	05.	1.40	N. X	*4000	.0023*	*6500	.0170	.0340	.0510	.0480	.0850	.1710	.2560	.3420	4260	00.13	1216.		03 50	,	65	1.40	1	*000	*0015*	*6200*	0600.	.0170	.0360	.0540	.0720	0060	. 1250	01810	0172	0254	.5500
å	• 35	1.69	800	-,1189	1043	-,1164	1347	-1703	1930	-1907	1882	1768	1713	1659	-1645		-1603		0 35		4	1.10	ě	1025	8080	0935	-1103	1235	1366	1348	1337	1327	-1302	1267	1736	-1700	1179
THE	0.00	93.70			2633										5786		.2984		THE		105	93.10		75/27	1227	4108	3246	.2218	,1389	.1503	.1571	.1633	.1794	.2014	.2213	25398	.2757
Ţ.	2.20	3.	907.00	14/1		9 0	£0.3		77.73	23.62	29-62	50.37	88.47		00.011	710/41	176.94		Ŧ,	7.50	u.	3.00		PC/PF	9		4 4	8.86	17.93	27.01	36.08	45.11	62.38	44.06	135.20	179.92	225.44

GROUP 3A

90/CX	RN/1N	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00		%3/0% 0.00	RN/IN .23	17 60.00 60.00 60.00 60.00 60.00 60.00
03/08	LENGTH 15.0	0.000 0.000 0.014 0.014 0.019 0.019 0.019 0.019		03/08 .20	LENGT: 15.0	
05.	6.1 1.40	AMF .0025* .0050 .0050 .0050 .1000		50	1.40	AMF .0009 . .0350 .0350 .0530 .5380 .5380
n* •16	PF 1.10	CPB 0934 1373 1373 1373 1233 1180 1110		0* •2A	4. 28.	CPA -1201 -1820 -1758 -1758 -1757
THEJ 23.30	10F 96.00	PB/PF -4109 -3148 -1346 -1526 -2667 -2547 -2562 -3304		1HFJ 3.00	10F 93.10	P8/PF • 4743 • 21034 • 22034 • 2401 • 2401
M.J. 2.20	MF 3.00	PC/PF 1.61 18.09 27.29 36.39 91.09 116.40 181.40	GROUP 4A	M. 2.70	NF 2.50	PC/PF 117.52 176.22 235.27 293.67 352.49
00°0	RN/1N	70.00 70.00 70.00 70.00 70.00 70.00 70.00	9	00°0	RN/IN .47	66 60 60 60 60 60 60 60 60 60 60 60 60 6
0J/DB .20	LENGTH 15.0	CT .069 .109 .149 .385 .385 .587 .587 .587 .587 .587 .587 .5977		03/08 •20	LENGTH 15.0	CT006* 006* 003* 003* 003* 008 06
60 • 50	63	RMF •0340 •0510 •0680 •1290 •1290 •2570 •2590		07 • 50	67	RMF .0009* .0023* .0023* .0035* .0178* .0178* .0230 .0230 .0350 .0590 .0590 .0590 .1160 .1760 .2360
0* •16	PF 1.69	CPB 1676 1929 1845 1795 1627 1627		0# •28	1.64	CP8 1173 1174 1014 1034 1034 1238 1386 1935 1935 1935 1935 1935 1935 1935 1935 1935
THEJ 20.70	TOF 108.70	PB/PF - 2667 - 1559 - 1925 - 2146 - 2146 - 2877 - 3157		THF.J 0.00	70F 93•10	PB/PF - 54864 - 5589 - 5559 - 5559 - 5581 - 1593 - 1593
2.20	2.50	PC/PF 11:83 17:81 23:79 44:59 59:35 18:76 116:60 148:34		2.70 2.70	2.50	PC/PF - 49 - 10 - 11 - 13 - 10 - 10

80/ra •25	LENGTH 15.0	
79°	1.40	### - 3700 - 5570 - 5570 - 7440 - 9290 1.0990
.35 •35	79. 28.	- 1201 - 1201 - 1762 - 1762 - 1709
THEJ 0.00	TOF 93.30	PB/PF -4741 -4741 -2290 -2407 -2519 -2519
м. 2•70	2.50	PC/PF 116.50 1175.68 175.68 235.07 293.34 147.13
0,00	RN/IN •23	71 C C C C C C C C C C C C C C C C C C C
03/08 •25	LENGTH 15.0	011*016*006*026*026*067108190
0) .62	6,1	.0015* .0015* .0034* .0186* .0340 .0560 .0560 .0560 .0560 .0560
. 3 f.	рЕ 1.69	CDB 1192 11016 11016 1193 1933 1933 1804 1780
THFJ 7.70	TUF 93.10	P8/PF 4787 4973 4021 1457 11541 11541 11541 11541 11550
#. 2.70	2.50	PC/PF 1 - 49 2 - 94 2 - 94 11 - 79 11 - 79 11 - 79 11 - 88 88 - 34 11 - 35 11 - 35 11 - 35

0* •28	44 55.	CP8 1289 1259 1259 1230		ET
14£J 0.10	10F 93.70	PB/PF -1873 -1961 -2267 -2157		THEJ 0.00 TOF 93.00
MJ 2.70	4F 3.00	PC/PF 183.74 270.05 360.05 560.25 563.90	GROUP 48	#3.2.30
00°0 0°00	RN/1N	U 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		XJ/DB 0.00 RN/IN
07/08 • 20	LENGTH 15.0	- 003* - 003* - 003* - 0048 - 0048 - 134 - 134 - 270 - 406 - 406 - 645 - 683 - 683		63/08 .25 LENGTH 15.0
	6J 1.40	RMF -00054 -00127 -0067 -0120 -0250 -0250 -0250 -0260 -1870 -1870 -2510 -3170		63 63 64
0* •28	PF 1.10	C C P R 1024 1024 1024 1024 1024 1024 1024 1024		0* .36 PF 1.69
THF.J 0.30	10F 93.70	08/PF .4594 .4594 .2395 .1226 .1226 .1359 .1559 .1561 .1661		THFJ J.J0 TUF 93.10
2.70	MF 3.00	PC/PF 918 4.53 4.53 11.99 11.99 27.99 8.95 6.55 90.93 11.95 11.95 11.95 12.85 13.95 14.95 15.95 16.95 1		2.70 7.70 7.50

GROUP 4A (Concluded)

90/CX	AN/1N .51	- 66644 - 66666	;	88	RN/1N	700000 70000 70000 70000 70000 70000
01/DB	15.0		2	. 20	LENGTH 15.0	0000 0000 0000 0000 0000 0000 0000 0000 0000
ro •••	07. 1.40		ā	.50	1.40	RMF .0025* .0240 .0370 .0370 .0950 .1260 .1380 .3150
0* •35	74 68.	CPB 1275 1275 1217 1217	ž	.28	PF 1.10	
1HFJ 3.20	10F 93.10	P8/PF - 1966 - 2223 - 2327 - 2443		10.00	10F 99.00	PB/PF •4142 •1158 •1158 •1383 •1617 •1655 •2065
LH 07.5	MF 3.00		GROUP 4C	2.70	MF 3.00	PC/PF 1.81 4.54 17.95 27.11 27.11 36.11 90.86 1135.63
00°0	RN/1N	00000000000000000000000000000000000000		0.00	AN/1N	7C 63.00 63.00 63.00 63.00 63.00 63.00
0.7708	LENGTH 15.0			• 20	LENGTH 15.0	
07 •62	1.40	RMF .0008# .0019# .00190 .0190 .0390 .0390 .0390 .1370 .1370 .1370 .2970 .3970	i	.50	63	RMF .0009* .0023* .0110* .020 .1400 .2340
0* •35	1.10	CCPB 	i	•28	PF 1.73	CPB11921058139920171939193919391939
THEJ 7.30	10F 93.10	PB/PF • 3548 • 24432 • 1196 • 1196 • 1197 • 1197 • 1193 • 1193 • 1937 • 1937	į	13.00	105 103.00	98/PF .4897 .5468 .4706 .4009 .1367 .1727 .2126
2.5 07.5	3.00	PC/PF • 39 • 50 • 50 • 52 17.69 27.03 36.09 62.33 90.41 135.21 130.45 225.96	;	2.3	NF 2.50	PC/PF .49 1.16 5.49 11:29 23:12 69:88 116.87 16:33

00°0	RN/1N	70.07	70.00	70.00	70.00	20.00	20.00	70.00	70.00	70.00	70.00	10.00	70.00	70.00			90/rx	RN/1N	2	70.00	20.00	70.00		20.02	70.00	10.00	10.00	70.00	70.00	20.00	70.00	20.00	70.00
07/00	LENGTH 15.0	CT 003*	0.000	020	970.	920.	261	201	. 271	607.	.478	.548	.687	. A08			03/08 .20	LENGTH 15.0	5	005	003	*000*	050	740	180.	•095	.123	-192	-262	084	.549	-689	£ .
ra •\$0	1.40	RMF .0012*	*005	.0120	•0520•	0370	0640	0460	1260	.1890	.2200	.2520	.3150	.3700			05+	1.40	R	*5000	*0013*	*0000	0000	0880	0380	•0460	0650	0060	1220	2210	.2530	.3160	0016
0. •24	PF 1•10	CP8 0910	0928	1200	1416	1398	7051	-1342	1332	1312	1295	1279	1254	1233			D* •28	PF 1-10	CPB	0993	0924	1032	1338	-1392	1383	1374	1358	132/	1310	1261	1243	1208	0511.
THFJ 15.00	105 133.30	PB/PF	-4148	.2435	1376	.1188	2621	1545	1606	.1731	.1839	1691.	96 (2.	.2231			THFJ 20.00	T0F 93.00	PB/PF	.373A	.4177	1446	1556	1227	.1285	.1340	.1442	1639	14/1.	2249	.2164	.2385	7007*
H.3 2.10	MF 3.00	74/2d		# C . E	18.06	27-11	30.27	0.000	91.15	135.97	158.61	181.55	226.96	266.57		GROUP 4E	M. 2 • 70	MF 3.00	PC/PF	.41		4. A	15.11	24-16	28.62	33.29	47.41	01.00	81.93	159.32	181.88	727.67	11.0407
KJ/DR 0.00	RN/1N -47	75.00	75.00	75.00	75.00	75.00	75.00	25.00	75.00	75.00	,						00°0 0°00	RN/IN .47	21	68.00	68.00	68.00	00.00	00.89	68,00	68.00	98*00	68.00	68.00	00.86	68,00		
03/08 •20	LFNGTH 15.0	CT 003*	.003	2,042	960	.186	.252	1981	515	244							03/08	LENGTH 15.0	13	*900*-	*500*-	**001*	*****	040	020	680*	•139	.144	.243	767	707		
رم 50	1.40 0.40	RMF .0023*	*6500	0230	0440	.0890	1180	0770	23.70	2960								1.40	A A	*6000*	.0016*	•0032#	*1*00*	0220	0360	•0440	.0670	•0700	1150	01210	.3260		
0. •28	PF 1.69	CP8 1029	1083	1425	2005	1957	1940	1000	-1840	1802	•						0* •28	PF 1.73	600	1196	1072	1069	6/01-	0171-	1885	2025	1995	-1999	1964	1863	1775	1	
14FJ 15•20	10¢ 110.00	PB/PF .5496	.5259	. 3765	.1224	.1434	1539	1868	1049	-2115							THEJ 20.70	107 103.00	PRIPE	.4877	.5476	.5417	4750	304.2	1913	.1311	.1442	.1424	1651.	1000	2408	!	
M.5 2.70	#F 2.50	PC/PF 1.19	2.97	20.71	23.69	44.44	19.37	20.00	118.47	148.15							Z. 20	MF 2.50	PC/PF	64.	8	1.63	9 6	7.5	18.20	22.33	33.77	34.93	57.39	114.47	162.91		

THE PROPERTY OF THE PROPERTY O

80/5x	N/1N .50	40.00 60.00	00.00	00.09	00,00	00.09	00.09	00.09						*		3	31/70	9	•	7	2,	•			•		,	•	•	•	•	•		,	•	•	•
07/08	LENG1H 15.0	, 000°	900	.015	.054	1111	•150	212.						•		2	ALC:NO	200	}	t	-001	005	900	.01	•016	120.	.031	040	•050	690.	•00•	.191	. 288	.385	.776	1.068	1.457
05. 05.	6J 1.40	.0017#	0000	00000	.0260	.0520	0000	0621.						ē	5 6	:	3	1.40	}	RAG	*000	.0022	•0040	0900	•0080	.0110	•0120	0610.	•0540	.0330	.0440	.0880	.1320	.1760	.3550	.4870	0499*
•58	4.	CP8 0701	0757	0773	0761	0728	0715	00						ć	.28	į	Ą	28	•	80.5	0557	0563	0585	0605	0610	0595	0597	0588	0586	0576	0567	0530	0515	0491	0469	0438	6040
THEJ 23.30	10F 95.00	P8/PF	.1512	1335	1470	.1843	1991	1667.						- 47.	200		105	00.0		PA/PF	2093	2008	.1694	.1414	.1353	.1556	•1529	.1653	.1681	.1835	.1954	.2478	*597*	.3331	.3345	.3779	2614
#,5 2.70	MF 4.00	PC/PF 2.26	6.80	11.31	33.57	66.86	89.63	190.09						*	2,70		I	4.50		PC/PF	1.23	39.6	7.12	U.C.	14.25	17.83	24.96	32.14	39.18	53.59	71.61	142.85	214.49	286.05	574.09	788.54	10/4.88
00°0	RN/1N	۲,	l i	۱ ۱	;	1	1		•	•		ı	1	•	•	•	•		,	•																	
03/08	LENGTH 15.0	003*	*600	- 001	* 000	.008	110.	10.	.021	.027	.031	.033	.043	090	.124	.189	.253	.512	• 106	• 965																	
07 • 50	1.40	.0006	*9000	.0015*	.0043*	.0050	0000	0000	0110	•0140	.0160	.0170	•0220	•0520	.0580	.0880	.1170	•2350	.3230	.4410																	
0* •28	94.	CPR 0836	0837	0780	0832	0895	-•0954	0465	0975	1002	1022	1029	1029	1020	0987	0959	6760*-	0401	0872	0829																	
	•	7	i	ii	i	i	•	, ,	,	•																											
THEJ 20.00	10F 0.00		2821					- 1717			.1 22 H	.1.69	.1169	.1253	.1529	•1769	.1856	•2266	.2515	.2891																	

00°0	44/1N	- 44 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	\$2*00 *7\D	0.00 RM/IN .23	000000000000000000000000000000000000000	
00/ru	LFNGTH 15.0	- 0111 - 0111 - 034 - 034 - 034 - 034 - 036 - 041 - 041	1.486 DJ/D8	•20 LENGTH 15•0		
£.	0 0	RMF .0012* .0050 .0500 .2230 .1080 .0500 .4530 .6650	0. 20	.50 6.1		
•0	 	C C C C C C C C C C C C C C C C C C C	1034 0	• 22 P F • 85	CPB 1197 1892 1876 1860 1847	
TMFJ 23.30	107.70	98/9F •36/74 •1043 •1869 •1214 •2956 •3266 •5155	.3550	0.10 10F 93.10	PB/PF -1761 -1772 -1791 -1916	
M. 5 - 70	MF 3.00	PC/PF 1.30 1.30 1.31 1.41 1.41 1.42 1.44	215.30 5 A	3.20 E.50	PC/PF - 49 1176-17 235-03 293-47 352-74	
			GROUP			
00°0	AN/1N	1C 67.00 67.00 67.00 67.00 67.00 67.00 67.00	90/c×	0.00 RN/1N .47	10 60 60 60 60 60 60 60 60 60	00.00 00.00 00.00 00.00 00.00
90/FG • 30	LENGTH 15.0	CT015* 009* -004* -091 -205 -673 -673 -1-121	17 PB	.20 LENGTH 15.0	.003* .003* .003* .016* .068*	.057 .074 .158 .241 .408
ια .τ.	6.1 1.40	AMF .0027* .0052* .0114* .0500 .1020 .5200 .5200	ā	63	RMF .0009* .0023* .0059* .0118* .0237*	.0310 .0390 .0780 .1170 .1560
•0•	PF 1.73	CPB 1200 1155 1155 1396 1779 1559	å	.22 pF 1.69	CP8 1190 1071 1176 1343	1485 1926 1912 1896 1890
THFJ 20.00	10. TOF	PB/PF • 4968 • 5533 • 5058 • 4046 • 1211 • 1613 • 30374 • 30310		0.70 10f 93.70	P8/PF -4740 -5311 -5313 -4852 -4852	.3507 .1562 .1577 .1772
2. 70	* \$. \$.	PC/PF .50 1.16 2.55 2.55 5.31 11.30 115.30 115.35 138.85	i	% ± %	PC/PF 1.18 1.18 2.95 5.91 11.85	23.62 29.55 58.97 88.44 117.90 1.7.34

GROUP 5A (Concluded)

00°0	25.	7C 00.00	00.09	60.00	200												80/FX	0.00	NI/NN	.47	٤	00.09	00.09	90.09	60.00	60.00	00.09	00.00	00.00		000	9	60.00
07,08	LENGTH 15.0	13.6	.526	. 703	288.	***											80/00	•31	LENGTH	15.0	;	-017	-010-	*600*	*240*	.109*	105		0.51		900	1,041	1.254
05°		RMF	2480	.3310	.4150	.4440											2	.79	ŝ	1.40	3	*005	*0900	.0150	.0301	*EU90*	0090	0620*	0660	0000	000	0.01	.5470
0* •22	7. 22.	840	1339	1318	1307	1249											ċ	.35	ā	1.69	ě	1193	8101-	1089	1300	1525	1954	1944	1922	1875	0001-	1001	1835
1HEJ 0.30	10F 93.10	PB/PF															THEJ	0.0	TOF	93.30	400	72/4	7715	.5234	.4313	.3324	-1447	.1491	.1539	.1796	1991	. A C	.1975
M.5 3.20	MF 3.00	PC/PF	178.60	360.43	451.45	545.05										P 58	3	3.70	T.	2.50	ě	44/14		2.95	5.89	11.80	17.75	23.60	29.47	58.72	16.88	16.711	176.49
															1	GROUP																	
00°0	RN/IR	1¢:	60.09	60.00	00.00	90.09	\$0°0¢	60.00	60.00	00.09	00.00	00.04	00.00	60.09				90/Cx 0*00	•	N 1 / N N	! !	5	60.00	00.09	00.00	00.00	00.04	•					
07/08	LENGTH		*500-	003*	*00.	020	740	.082	.116	.172	.260	.349	•438	.527				13/08 • 31		LENGTH		5	017	.827	1.248	1.671	2.283	707.7					
rg • \$0	3	1	.0005	.0012*	*0062*	*C210*	0540	.0410	.0570	.0830	.1240	.1660	.2070	.2490				5,		3,	•	RMF	*0025*	.3970	.5940	.7920	0166	1.00					
D*	4	01.10	2007	0929	0982	1110	1507	1396 -	1388	1383	1374	-,1364	1353	1343				*0		u l	68.	6.0	1200	1863	1849	1833	1814	-1809					
THEJ	104	93.00	PB/PF	4145	.3811	3005				.1286	.1339	.1405	.1471	.1535				¥		105	93.10	30/40	6749	1846	1976	1401.	2902	. 20 9R					
3 /	¥	3.00	PC/PF	9	4.52	9.01	18.02	100	62.45	95.59	135.30	80.58	225.68	271.73				₹,	5	#	2.%	30, 70	֭֭֭֭֭֭֭֭֭֭֓֞֝֝	117.49	175.73	234.21	292.94	318.66					

GROUP 5B (Concluded)

x3/04 0.00 4N/14	20000000000000000000000000000000000000	90°0 90/fx	RN/1N	70.00 70.00 70.00 70.00 70.00 70.00
63706 • 31 14867~	1. 1.1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.1. 1.1.	03/08 •20	LFNGTH 15.0	0 0000 00000 00000 0047 0047 0047 0047 0
2. 3.	. 424.0 . 6424.0 . 4440.0 11.0600.0 12.2720.0	ta 05.	63 1.40	. 000%. . 00160 . 0050 . 0050 . 0030 . 0050 . 1050 . 1050
5. 4.	111111111111111111111111111111111111111	D.	PF 1.10	CPR 0935 1955 1420 1420 1420 1356
146J 3.30 106 93.30	7476 17776 1974 1974 2049	THE, 23.30	10F 97.00	7007 1000
# 3.20	PC/PF 1#3.78 1#3.78 369.81 451.57 541.52		4F 3.00	PC/PF 10-31 10-31 20-55 20-55 20-55 10-13 10-65 20-13
		GROUP 5C		
83/08 0.00 RN/18	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	xJ/D8 0.00	RN/1N	70.00 70.00 70.00 70.00 70.00 70.00 70.00
1)708 .31 LFNGTH 15.0		63/88 •20	LFNGTH 15.0	C1 .069* .069* .158 .117 .159 .243
5. C.	RMF .0013. .00118. .0160. .0160. .0420. .0420. .0430. .1060. .2120. .3170. .510.	.00 •50	1.40	.02574 .03574 .0310 .0590 .0780 .1180
0. 3. 1.10	CP8 	0. •27	14 1.69	-1326 -1529 -1629 -1626 -1933 -1955 -1955
101 0.30 101 101	74.4. 74.4.	14FJ	10F 138.30	PB/PF -4194 -3747 -2884 -1364 -1366 -1643 -1768
3.70 3.70 3.70	PC (9 4 4 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	7.	2.50	PC/PF 11.91 17.85 23.83 44.57 44.57 69.43 89.10 118.64

THEJ 20.30

TOF 138.30
PB/PF -4711
-4249
-4249
-1385
-1385
-1385

GROUP 6A

. '.	# 4 		,	(it 1		<u>.</u>	2.		•	00.					;	5		z e e e	i	. :	000	3	00	00.4	00	00**.	00**				
			~ **.	¥:		0 6	- 0	3 4	4		- •	٠ ـ	 .		,	e : .		**************************************	•	• :					. 47. 4	271	**	-			
3	3.	Ì	.000			4474	0.40		## P	Į.					•	; \$		3 }	ļ				-010	. 0.00		****	444				
• •	**	ŝ	1122		1404	1997	- :776	1762	1736	### ### ### ### ######################					į	2 =	1	*	į				20710	*	3	- 1	1672				
7ME 20.00	10F									***					1	20.00 20.00		,				6327	4992	3928	-2962	-2050	.1720				
M. 2.70	MF 2.50	PC/PF	60.0	20.63	30.73	40.86	51.63	61.64 61.64	61.65	162.00						2.70		NF 2.50		#C/P#	6	3 2	20.02	91-50	E407 /	118.21	152.71				
09*0-	RN/IN	10	75.00	75.00	00.55	75.00	75.00	75.00	75.00	75.00					x3/08	00.0	RM/1M	.55	77	75.00	75.00	75.00	72.00		75.00	75.00	75.00	75.00	75.00	75.00	75.00
0J/D8	LENGTH 15.0	5	005	000	0520	1104	.087	•110	•110	•121					90/00	•10	LENGTH	15.0	5	0017	001	6003	0000		450.0	1087	•120	.166	860*	121.	.166
67.	100	RMF	.0003	0103	•0258	.0512	*040	•0512	•0512	•0766					2	•25	3	1.40													•0766
•14	PF 1.96	668	1111/	1314	1589	1545	1570	1545	1934	-• 1495					*0	•1•	PF	1.96	(P8	1136	1116	1907	-1224	1318	1545	1873	1980	1948	1950	1975	1940
THE 3	10F 95.0	P8/PF													THEJ	20.00	10F	95.0													.1420
MJ 2.70	MF 2.50	PC/PF	2.02	20.68	51.66	102.43	19.19	102.45	16.22	47. CC1					3	2.70	Ŧ	2.50	PC/PF	64.	56.	000	10.0	30.56	51.27	61.20	111,00	152.61	91.43	112.37	153.22

GROUP 7A

407.	21.44			
3.	=			
ä	3,	1600704666	7 7	
\$ -	*:			
1MEJ 20.00	104	**************************************	106 107 107 108 108 108 108 108 108 108 108 108 108	
# 2.70	MF 2.50	PC/PF 5.51 20.40 20.40 66.26 66.26 111.11.74 111.74 111.74	2 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 -	
99/FX	RN/1N •55	71 25 20 20 20 20 20 20 20 20 20 20 20 20 20	X X X X X X X X X X X X X X X X X X X	75.00
03/08 •10	LENGTH 15.0	CT 0002 0003 0054 0054 0121 1127 1127	DJ/DB 10 10 15.0 15.0 15.0 10.03 10.03 10.03 11.3 11.3 11.3 11.3	•057
67 •25		0002 0002 0002 0002 0002 0002 0002 000	00003 00003 00003 00003 00003 00003 000003 000000	
***	PF 1.96	CPB 1125 10037 16073 1702 1702 1702 1519	De D	1503
THE.)	10F 95.0	PB/PF	1HEJ 20.00 20.00 10F 95.0 95.0 98/PF 9529 9378 9378 9378 9378	
MJ 2.70	MF. 2.50	PC/PF 2 49 2 001 2 004 5 101 81 11 111 71 115 2 52 117 2 89	AL 2.10 2.10 2.50 2.50 PC/PF 5.51 5.51 5.65 111.77 111.77 15.65 76.92	54.49

44.00000000000000000000000000000000000	\$2
2	00. 00. 00. 00. 00. 00. 00. 00. 00. 00.
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	CPB PF CPB
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	THEJ 20.00 20.00 10F 10F 95.0
2.70 2.70 7.50 1.00 2.00 1.00 2.00 1.00 1.00 1.00 1.0	M. 2 - 70 M. 5 - 70 M. 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6
X	XJ/DB ND NJ/DB NJ/DB NJ/DB NJ/DB NJ/DB NJ/DB NJ/DB NJ/DB NJ/DB NJ/DB NJ/
01/08 •20 LENGTH 15.0 CT •005 •013 •047 •058 •047 •058 •0810 •126 •349 •4840 •6490	DJ/DB -20 -20 -20 -20 -007 -007 -003 -014 -213 -48 -648 -648 -170
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DJ CJ CJ CJ CJ CJ CJ CJ CJ CJ C
00. 00. 00. 00. 00. 00. 00. 00.	D*
THEJ 20.00 10.00 10.00 95.00 95.01 95.01 95.01 95.01 95.01 95.01 95.02 95.03 9	THEJ 20.00 20.00 1
MJ 2.70 1 1 2 450 PC/PF	MJ 2 - 70 2 - 50 7 - 50 1 - 51 1 - 51 2 - 61 2 - 61 2 - 61 1 - 61 1 - 61 2 - 61 1 - 61 1 - 61 2 - 61 1 - 61 2 - 61 1 - 61 2 - 61 3 - 61 2 - 61 3 - 61 2 - 61 3 - 61 3 - 61 4 - 61 5 - 61 6 - 61

GROUP 7B

\$4.00 0.50	***	\$400 2000 2000 2000 2000 2000 2000 2000	**************************************	2466838 2466838 2466838	95° C	1666666
wa/ra	15.0	20000	**************************************		07.00 07.00 1.00 1.00 1.00 1.00 1.00 1.0	
ري. 90•	3.	.0010 .0020 .0101	1678 1678 2240 27477	00000000 110000000 1100000000000000000	£9.	
•58	PF 1.96	1 - 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1508 1018 1785 1649	11.1.1 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.0000 10.000	0. •28	1 9 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
1HEJ 20.00	10F 95•0			. 2304 . 3118 . 3118 . 3138 . 2770 . 2613 . 2107	1HEJ 20.00	9550 PR/PF • 54940 • 54940 • 5295 • 2097 • 3102
2.70	MF 2.50	PC/PF 1.01 5.06	30.59 51.26 81.30 111.84 148.66	200.25 200.45 20	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2.550 PC/PF 1.01 1.01 2.00.47
x;/08 0.33	RN/1N	75.00 75.00 75.00	75.00		XJ/DB 0.82 RN/IN	25. T.C. 25. 00. 00. 00. 00. 00. 00. 00. 00. 00. 0
0J/08 •20	LENGTH 15.0	-0007 -00050 -0131			5J/58 •20 LENGTH	15.0 CT -0007 -0105 -013 -0125 -2125 -2148 -483 -650
65.	1.40	RMF •0010 •0020 •0101	. 1025 . 1025 . 1627 . 2242 . 2946		05. L0	RMF • 0010 • 0020 • 0010 • 0612 • 1627 • 2239 • 3000
0* •28	PF 1.96	CPB 1098 1036 1119	- 1901 - 1901 - 1901 - 1703		0. • 2.8 P.F.	1,96 CPB -1096 -1032 -1185 -1859 -1659 -1659 -1659
THE J	TOF 95.0	P8/PF •4994 •5178 •4899	1206 1337 1745 1240		THEJ 20•00 TOF	95.0 pn/pr .5297 .6066 .5297 .2739 .1664 .2767 .3261
2.70	MF 2.50	PC/Pr +49 1-02 5-07	20.59 20.59 51.18 81.21 111.91		2.30 AF	2.50 PC/PF .51 1.01 5.07 20.46 30.57 30.57 81.22 111.81

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GROUP 78 (Continued)

ACTOR NELWS	~ : : : : : : : : : : : : : : : : : : :	804 174 804 174 804 174 804 174
03/08 •\$0	 	02/08 •20 LENG 14 15.0 C1 •004 •191
رو. (و. بي)	8 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	050 6J 1040 1040 8MF 8MF 90006 90006 90006
0. •28 pF	C C C C C C C C C C C C C C C C C C C	D*
THE J 20.06 TOF		THEJ 20.00 10F 95.00 PB/PF 1903 -2579 -2969
MJ 2.70 MF 3.50	PC/PF 231.057 231.057 231.057 231.057 317.581 317.581	MJ 2.70 MF 4.50 PC/PF 1.75 77.24 142.78
XJ/DB 0.67 0.67 RN/IN .55	75.00 75.00 75.00 75.00 75.00 75.00 75.00	7.7.008 -1.20 -1.20 -50 -1.1 -1.1 -1.1 -1.1 -1.1
63/08 •20 LENGTH 15•0	CT -0005 -0005 -0008 -00	DJ/DB XJ/DB *20 -1.20 1.20
67 67 67	RMF • 0010 • 0010 • 0100 • 0410 • 0453 • 1623 • 1626 • 3032	DJ (6 6J (1 13-40 RMF 00290 00580 00580 01170 0170 0170 0170 0170 0170 0170 0170 0170 0170 0170 0170 0
24 •28 PF 1•96	10000000000000000000000000000000000000	0.28 0.28 0.69 0.09 0.0032 0.0032 0.0032
THEJ 20.00 TOF 95.0	PB/PF • 51995 • 5296 • 25916 • 2591	1HEJ 20.00 10F 95.00 98/PF -2926 -3430 -3430 -3430 -3458 -4580 -4868
MJ 2.70 MF 2.50	PC/PF - 50 1 - 50 2 - 50 2 - 50 2 - 50 3 - 50 3 - 50 5 - 60 5 - 60 6 - 10 6 - 10 6 - 10 6 - 10 6 - 10 7 - 10 8	MJ 2.70 MF 3.50 PC/PF 57.42 57.42 86.442 14.96 230.28 316.72 431.52

XJ/DB -1.20	BN/IN	X11111111
07\08 •20	LENGTH 15.0	001 0001 0094 191 191 10068
09. •50	1.40	RMF • 0007 • 0040 • 0080 • 1760 • 0080 • 3950 • 6640
0* •28	₽£ •28	CPB -0554 -0572 -0436 -0495 -0495 -0439
THEJ 20.00	TOF 95.00	PB/PF •2150 •2487 •3824 •3824 •4376 •4773
2.70	₩. 00°	PC/PF 1.30 71.45 143.00 285.99 142.82 572.55 187.43

22

MJ 2.70 MF 2.50 PC/PF 10.41 20.69 30.82 81.81 81.83 135.63

GROUP 7C (Continued)

36°C-	# * * * * * * * * * * * * * * * * * * *	J 6	00.4	00.6	13.00	4.00	8	2	2000		8	2	19.00	2	8.5	25.00	•	0.10	## / ##	*	2						40.64	3.5	14.00	8					
#0/F0	15.0	***	011	.00.	100	0.20	780	55.5				6.5		687	1.092	1.235	900	98.	LEMOTH	15.0	5	013	0.0	-00	.132	106	. 198	.184	.263	7	76	7007	1.939		
54.	1.40 1.40	RMF	6 400	1000	•0126	6220	7 6 6 6	10.00	***	5650	0000	0767	****	+368/	• 5067	.5721	ĉ	3. ·	ÿ	1.40	A A	• 0022	.0047	0440	9090	•0586	•0814	•0933	.1385	9666	16676	2000	•6.58		
• • •	рғ 1.96	CPB	-0038	1000	1056	1204		1,100		000		10.10	06:10	0641	1418	1389	ż	• 45	ğ	1.96	840	1049	0955	~.1523	1480	1345	1588	1726	92/10-	1010	1206	0914	0733		
	10F 95.0																THE	20.00	105	95.0	PB/PF	.4951	• 5404	.2673	.2878	.3529	•2359	1693	.1693	2722	4107	1095	•6475		
MJ 2.70	MF 2.50	PC/PF	66.	2002	2.81	20.00		12.00		100	7 · · · · · · · · · · · · · · · · · · ·	10000	11.10	01010	112.39	126.91	***	2.70	**	2.50	PC/PF	50	*6° 7	10.43	15.45	12.99	18.07	20.71	30012	51.73		112.43	136.60		
xJ/D8 -0.20	RN/IN .55	77.	75.00	75.00	15.00	75.00	200	15.00	75.00									XJ/D6 0.33	7.	. 55	:	ء -	000	24.00	24.00	75.00	75-00	75.00	75.00	75.00	75.00	75.0	20.00	200	75.00
90/га	LENGTH 15.0	CT	104	.307	-517	215	218.	1.124	1.368								4	90/50		15.0	ţ	- 20	010	1057	280	801	.132	.133	.159	.185	•285	927	757		1.312
.0 .75	1.40	RMF	•0213	•190•	-1037	1601	2401.	66779	• < 133								;	27.		1.40	4		7,000	0353	0440	0586	9090	1690	•0818	•0934	0661.	. 2250	3446	5065	.6067
0.44	PF 1.96	CPB 1457	1746	1615	1529	1305	1306	1304	14314								ż	.45	u d	1.96	agu	9,00	0000	1320	-1570	1629	1700	1699	1740	1678	1822	1621	1587	1403	1241
THEJ 20.00	10F 95•0	PB/PF	.1598	•2229	*2644	1286	2776	8204										20.00	105	95.0	BH / DF	4057	5603	3640	-2445	-2161	.1817	.1825	•1629	-1962	1231	.1771	2365	.3249	.3786
MJ 2.70	MF 2.50	PC/PF 7.95	10.64	30.95	70.10	82.13	112.63	136.95									i	2.70	¥	2.50	PC/PE		1.05	7.84	10.42	12.99	15.44	15.46	18.51	20.72	30.04	52.33	76.45	112.31	134.60

GROUP 7C (Continued)

\$0/0% 0.88	##. #	:	19.00	000	2000		13.00	19.00	75.00	75.00	75.00	79.30	78.00	70.00		90°0	1			~	69.00	65.00	65.00	63.00	63.00	62.00	9 200	00.60	92.00
60/00	15.0	t)	•00	200	601.	.163	1320	*085	.285	• 584	0.89	. 7840	1.092	1.7.8		80/ru .25	7,010	15.0		t	011	60.0	.237	•399	• 399	109	908	~ .	1.217
54.	1.60	A.M.F.	.000	96.00	\$6.60	.0816	•060	0440	0 1 4:00	9.00	2355	. 3674	-5067	.5772		59°		3.5		II CC	•0016	05.60	•0931	1862	.1865	.2801	.3735	.3756	.956.
***	pr 1.96	8 C	-,1045	1548	1751	1767	1564	-•1492	1636	1634	1415	-1079	2742	0575		0. 9.352	ŭ	0.85		840	1197	1891	1899	1845	1844	1805	1791	1791	1759
1HEJ 20.00	10F	PR/PF	F764*	2560	.1574	•1495	•7472	-2817	•7125	• 137	• 3189	• 4806	•643]	.7234		1HEJ		95.00				.1723							
2.70	MF 2.50	PC/PF		13.00	20.71	18.55	15.41	10.43	30.84	30.78	51.51	81.50	112.40	127.16	€	# 5	•	2.50		PC/PF	.51	17.75	29.52	20.65	59.12	88.79	118.37	119.04	177.34
															GROUP														
XJ/DB 0.67	RN/IN	• 55	J.	75.00	7.00	75.00	75.00	75.00	75.00	75.00	75.00	75.00	75.00	75.00		90/FX 0°00	3	•12	7	65.00	65.00	65.00	65.00	65.00	65.00	65.00	65.00	65.00	
03/08 •30	LENGTH	15.0	t	0110	0000	750	132	.1592	. 1844	.284	.493	•180	1.092	1.315		80/L0 85*	7	15.0	t	011	.117	.231	•233	.396	•556	₹0₽*	-805	1.216	
24.	3	1.40	RMF	9400	. C.	.0354	-0695	.0819	•0634	•1388	•2339	.3686	-5067	.6081		5J • 628	;	1.40	RMF	•0016	9650*	.1118	.1124	•1869	.2610	•3725	•3756	• 5595	
D*	4	1.96	CP6	0953	1511	1368	1462	-,1528	1749	1622	-,1375	1080	0742	0495		0 * • 3 5 2		0.42	68	1248	1824	1792	1794	1772	1764	1740	1741	1732	
THEJ 20.00	10F		PB/PF										.6430	. /618		1HEJ 0.00		95.00	PB/PF	.4539	.2017	.2158	•2147	•2245	.2751	.2383	.2378	•2418	
2.70	T.	2.50	PC/PF	1.01	10.43	7.855	15.67	18-16	29.71	30.79	51.88	81.77	112.41	134.89		M.)	;	2.50	PC/PF	• 52	18.92	35.42	35.62	59.24	82.73	118.06	118.23	177.58	

#0/r*	#	8 677	8 . ž.	Maria 112	2888888
80/rg	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	88/79	.096 LEMGTH 15.0	LENGTH 15.0	0.000000000000000000000000000000000000
	1001 00016 0000016 0000000000				0000 0000 0000 0000 0000 0000 0000 0000 0000
	CPB	å			######################################
1HEJ 0.00	95.00 PR/PF • 4806 • 1436 • 1953 • 1953 • 2200 • 2290 • 2390	THE		۰	PB/PF -4765 -2302 -2912 -2909 -3831 -8831
2.5. I	2.50 PC/PF 17.55 44.34 58.99 58.99 58.99 118.06 118.06	7 m	MF 2.50	AF 2.50	200.00 200.00 200.00 200.00 200.00 200.00 200.00 200.00 200.00
		82 97			
		GROUP			
XJ/DB 0.00 0.00	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	9 ea/rx	RN/IN •23	. 12 TC	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
03/08 •25 LENGTH	- CT - CT - O11 - 112 - 396 - 593 - 593 - 666 - 906 - 1066	80/C0	LENGTH 15.0	15.0	000000000000000000000000000000000000000
62.8 64.6	RMF • 0016 • 0576 • 0576 • 1870 • 2491 • 2491 • 3133 • 3135	3. **	34.	1.40 RMF	.0000 .0006 .0006 .0016 .0023 .0031
0. .352 PF	CPB 1184 1941 1941 1816 1816 1801 1745	• 1 ♦	74 0.85 74	0.42 CPB	1196 1516 1620 1620 1609 1410
1HEJ U.00 10F 95.00	P9/PF •4819 •1504 •1964 •2053 •2053 •2053 •2120 •2181	1HEU 0.00	70F 95.00 70F	95.00 PB/PF	.4765 .3365 .2302 .2911 .2909 .3401 .3831 .3830
MJ 2.70 MF 2.50	PC/PF • 50 18-13 18-25 59-27 79-00 79-00 98-67 118-37	¥.0	2.50	2.50 PC/PF	17,94 17,94 1,94 1,94 1,94 1,94 1,94 1,94 1,94 1

CROUP 98 (Centinued)

ĸ	THEJ	D●	0.1	03/08	XJ/DB
1.00	0.00	•14	.14	.056	6.00
HF	TOF	PF	ری	LENGTH	MN/IN
2.50	95.00	1.27	1.40	15.0	.35
PC/PF	PB/PF	CPB	RMF	ĊT	tc
.51	.4840	1179	•0001	0000	65.00
18.10	. 3286	1534	.0005	.001	65.00
18.16	.3285	1534	-0005	•001	65.00
18.16	.3285	1534	.0005	.001	65.00
59.33	.2851	1633	-0016	•003	65.00
78.95	• 7246	1543	.0021	.005	65.00
79.45	.3244	1544	•0021	.005	65.00
99.04	-3558	1472	•0026	.007	65.00
146.58	-4158	1335	•0036	•010	55.00
177.17	.4505	1255	•0047	.012	65.00

MJ	THEJ	D#	ĐJ	DJ/DB	XJ/D8
1.00	0.00	•14	.14	•056	0.00
MF	TOF	PF	GJ	LENGTH	RN/IN
2.50	95.00	1.70	1.40	15.0	•47
PC/PF	PB/PF	CPB	RMF	СĪ	TC
17.66	•3316	1527	•0005	•001	65.00
.48	.4809	1186	•0000	•001	65.00
44.25	•2522	1709	•0012	•	65.00
44.25	.2522	1709	.0012	.003	65.00
58.1:	.2870	1629	•0016	.004	65.00
59.44	.2874	1628	.0016	.004	65.00
88.50	•3371	1515	•0023	.006	65.00
118.02	.3787	1419	.0031	.008	65.00

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Redstone Arsenal, Alabama 35809		N/A	
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C. E. Brazzel			,
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None	Same as N	io. 1	
Results of supersonic wind tunnel tes of varying nozzle geometry, location, and su cylindrical body at zero angle of attack. The the parametric influences in the regions whe which occurs in the lower range of thrust lev experimental results is also included.	upply pressur e purpose of (are base press	e on the ba the tests wa sure is nea:	se pressure of a as to investigate r a minimum,

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LINK B LINK C **KEY WORDS** Supersonic wind tunnel tests Nozzle geometry Location Supply pressure Cylindrical body

UNCLASSIFIED

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Security Classification